

# Electron Gun (source)

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**July 30<sup>th</sup> , 2025 at OCPA Accelerator school, Thailand**



- Introduction
- Some topics in electron gun
- Typical guns for accelerator facilities



- Some materials for this lecture is literally taken from talks / reports / papers / notes from a large number of people
- Stimulating discussions with many colleagues and friends in the **electron source / accelerator / ultrafast science** communities over the past many years
- References:
  - An Engineering Guide to Photoinjectors
    - <https://arxiv.org/abs/1403.7539>
  - Several USPAS courses / lecture notes
    - <http://uspas.fnal.gov/>
  - Photocathode Physics for Photoinjectors Workshop series
    - Both in U.S. and Europe
  - Tons of journal and conference papers



半亩方塘一鉴开，  
天光云影共徘徊。  
问渠那得清如许？  
为有源头活水来。

—— 朱熹《观书有感》

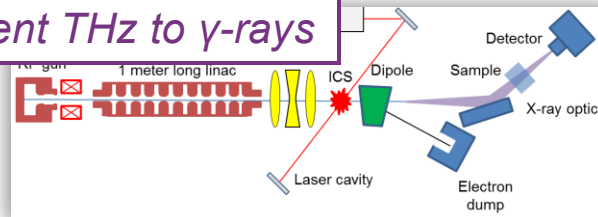
“源对装置的性能有决定性的影响”



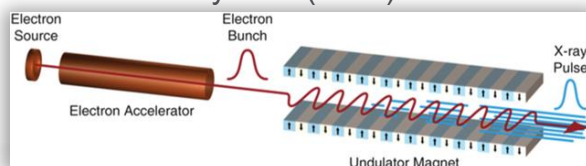
# E-beam-driven facilities and instruments

## Photon sciences: coherent THz to $\gamma$ -rays

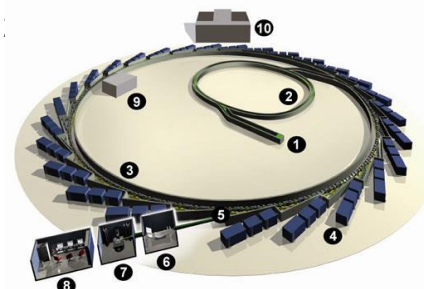
PRSTAB 17 (2014) 1.



Rev. Mod. Phys. 88 (2015) 015006

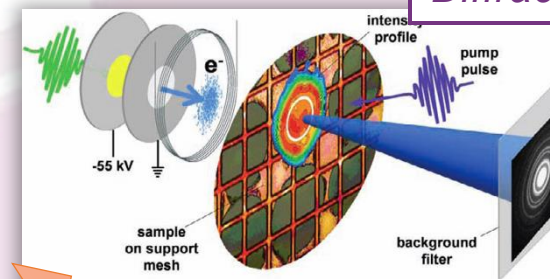


## Industrial applications: Nondestructive testing, therapy, irradiation

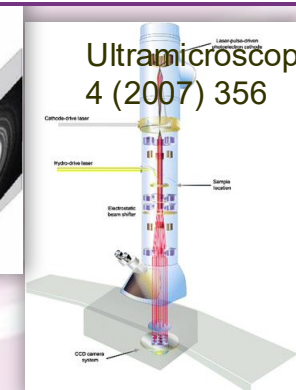


Electrons  
sources

## Electron scattering: Diffraction, imaging, EELS

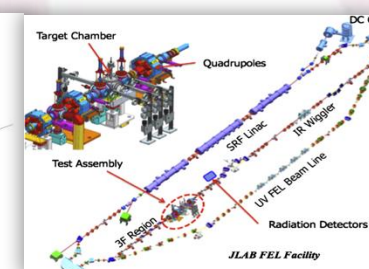
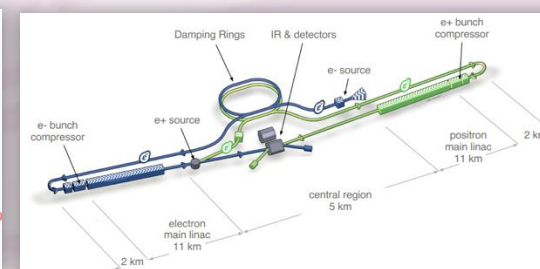
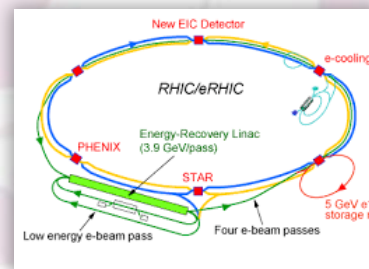


Science 323,  
1033 (2009)



Ultramicroscopy  
4 (2007) 356

## High energy physics: Colliders, dark matter search



<https://www.bnl.gov/rhic/news/081407/story1.asp>

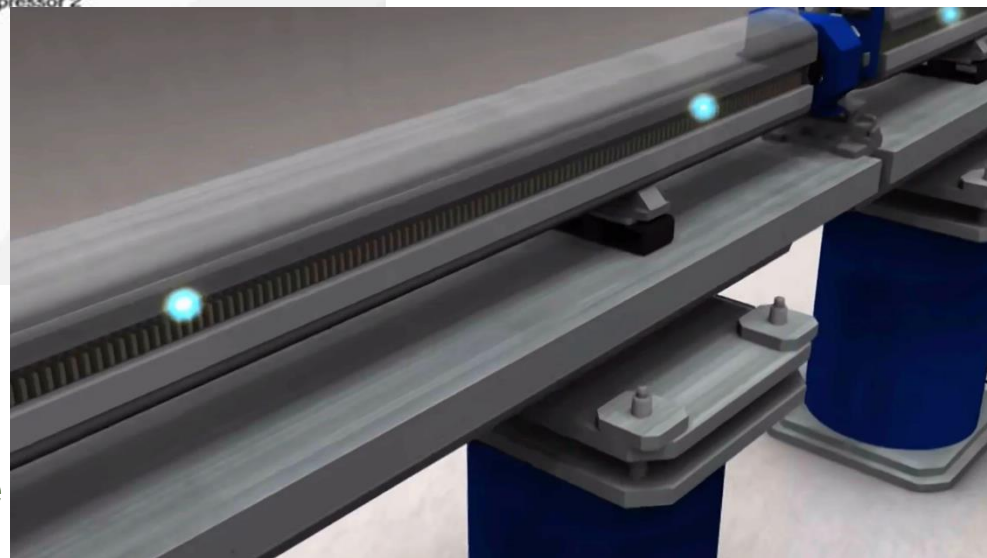
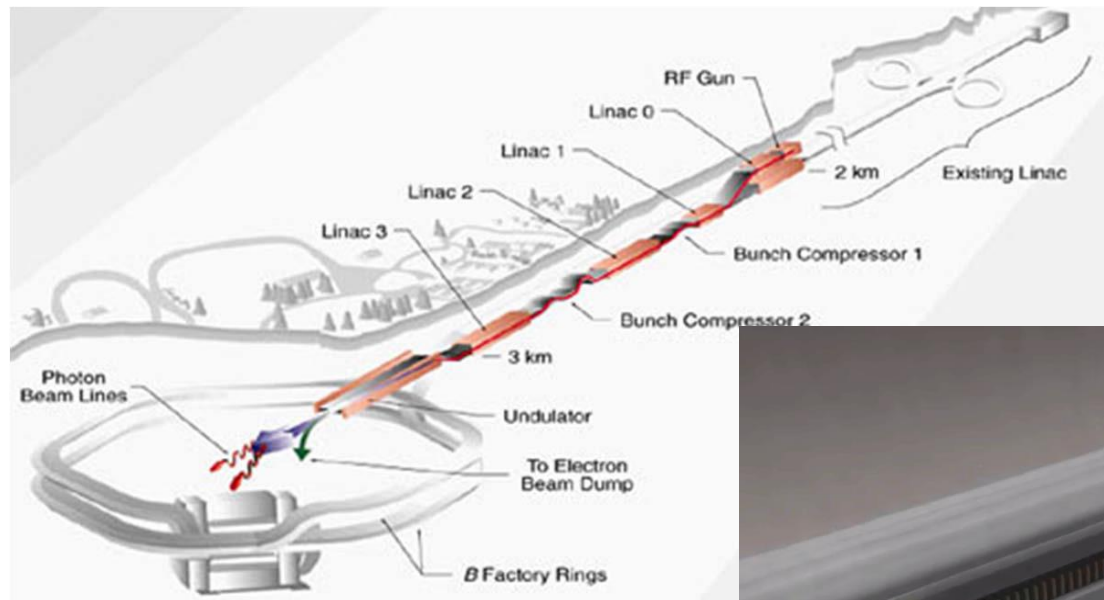
ILC CDR

NIMA 729 (2013) 69





- Advanced electron sources is one of the enabling technologies for the XFEL
- Photoinjectors delivered the required high brightness beams

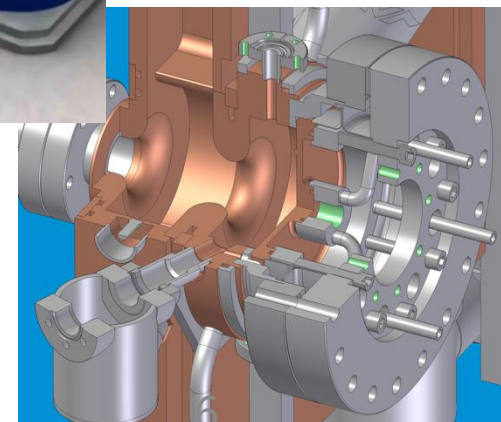


## Demands:

- Ultralow normalized emittance
- High current (kAmp)
- Beam charge ranging from 10 pC - 1 nC

$$\rho = \left[ \frac{1}{16 I_A} \frac{I_e K_0^2 [JJ]^2}{\gamma_0^3 \sigma_x^2 k_u^2} \right]^{1/3}$$

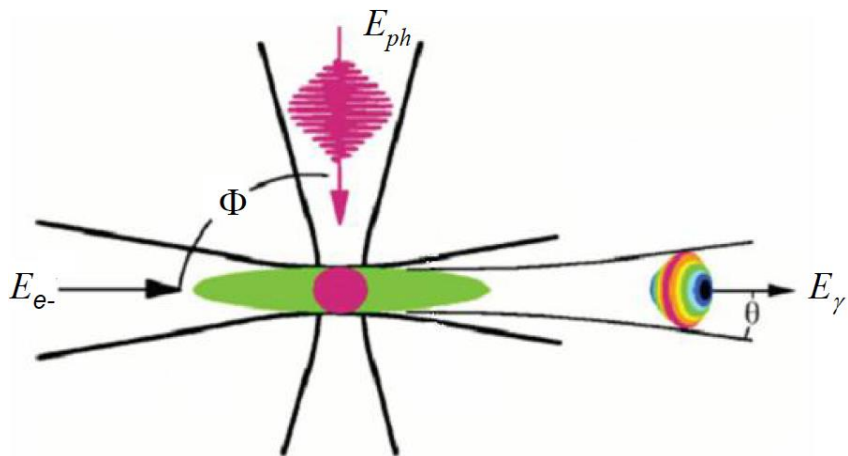
$$\frac{\epsilon_n}{\gamma_0} \leq \frac{\lambda}{4\pi}$$



*Photoinjectors deliver required e-beams for FEL*

Cut-away view of the LCLS gun. Courtesy of E. Jongewaard

# Inverse Compton scattering sources



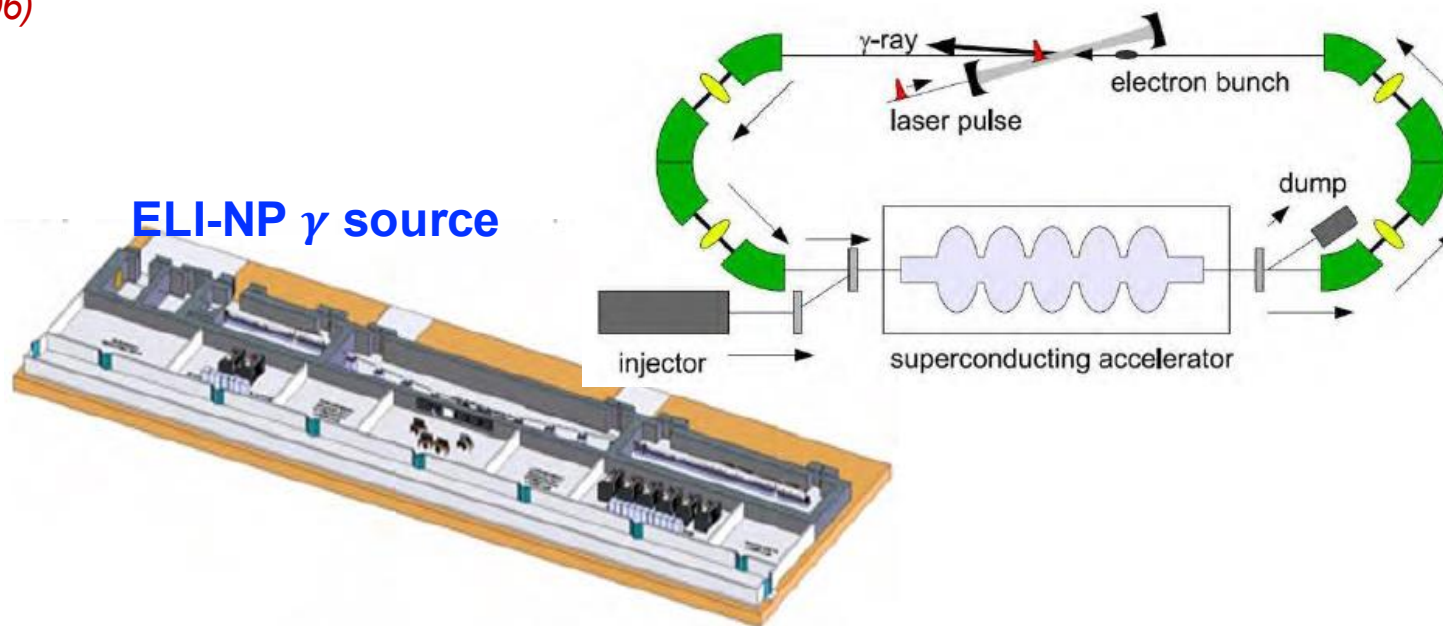
*R. Schoenlein et al., Science 274, 236 (1996)*

*Y. Du et al., RSI 84, 053301 (2013)*

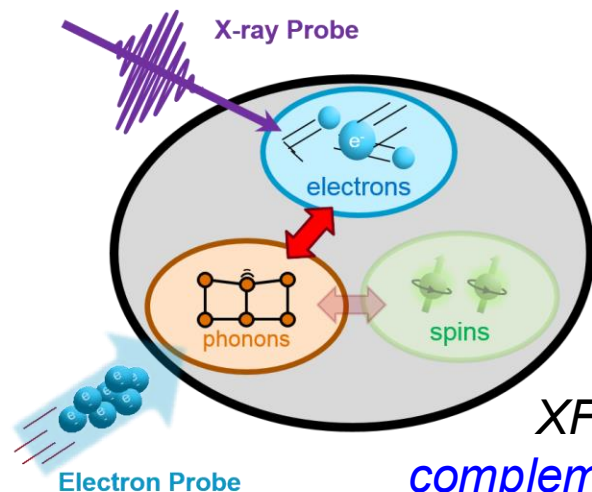
- Most promising approach for generating ultrafast **gamma-ray** pulses, for the emerging field of nuclear photonics
- Requires **high intensity, small spot, low divergence, ultrashort, well synchronized** electron and laser beams

## Demands:

- Ultralow normalized emittance ( $\sim 1$   $\mu\text{m}$ )
- Beam charge from 100 pC - 1 nC



## Visualizing the ‘ultrasmall’ and ‘ultrafast’



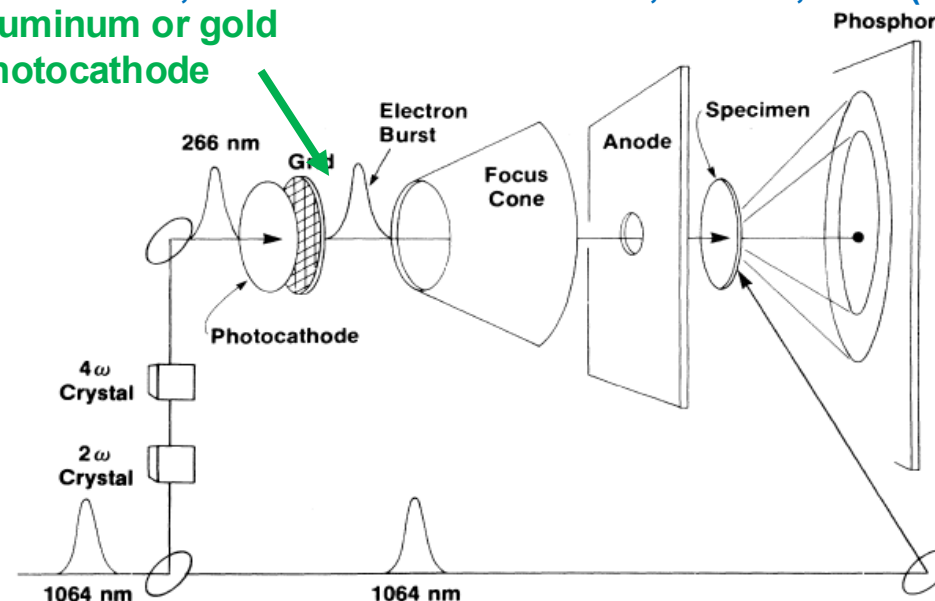
*XFEL and UES are complementary tools towards a complete picture of dynamics*

### Demands:

- Ultralow normalized emittance (nm rad)
- Ultrashort bunch length, ~10's fs
- well synchronized to laser with in 10-100fs
- Beam charge from fC - pC

G. Mourou and S. Williamson, APL 41, 44 (1982)

S. Williamson, G. Mourou and J. C. M. Li, PRL 52, 2364 (1984)  
aluminum or gold photocathode



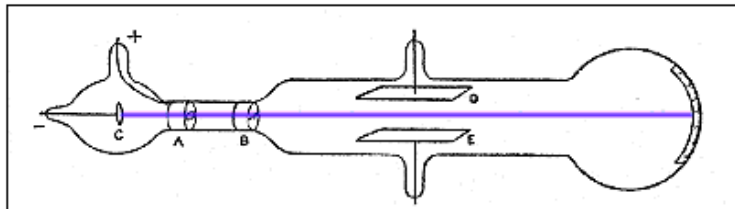
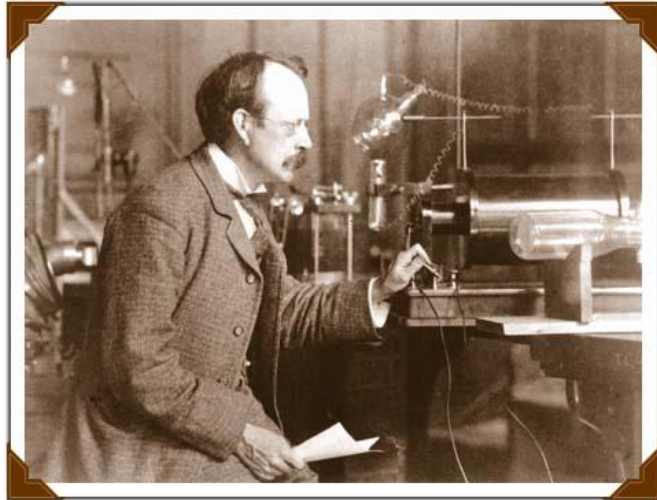
### Science outcome:

See e.g. M. Chergui and A. H. Zewail, *ChemPhysChem* 10, 28 (2009); R. J D. Miller, *Science*. 343, 1108 (2014) and etc.



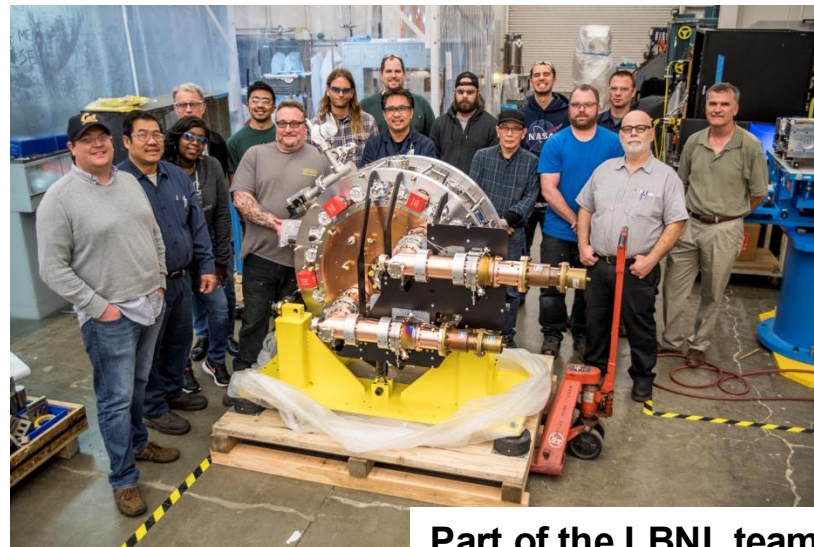
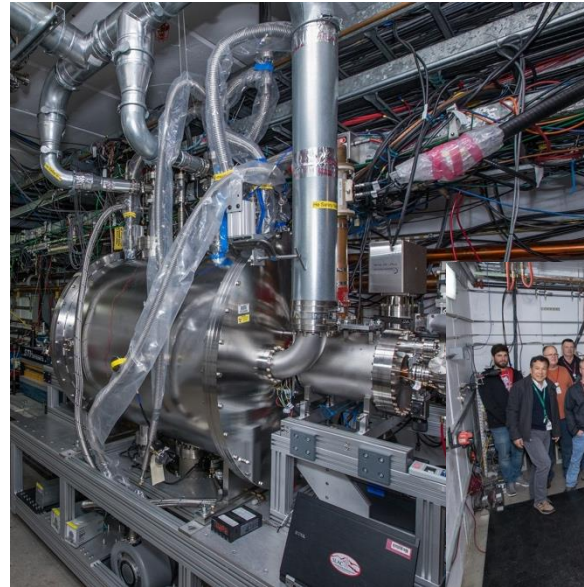
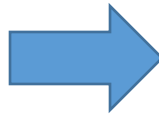


# 100+ years development of electron sources

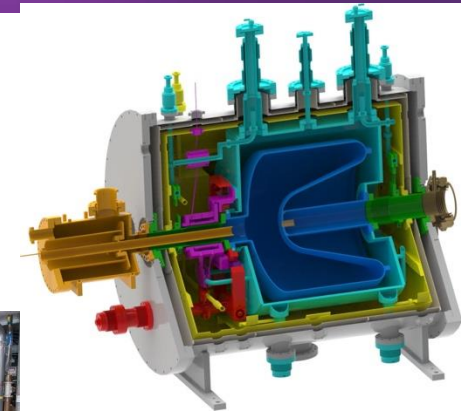


Crookes-Hittorf tube

J. J. Thomson, discovered electron using a cathode ray tube (1897)

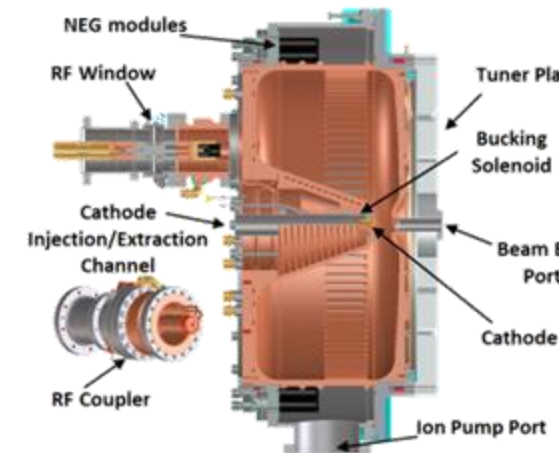


Part of the LBNL team and the LCLS-II gun (2017)

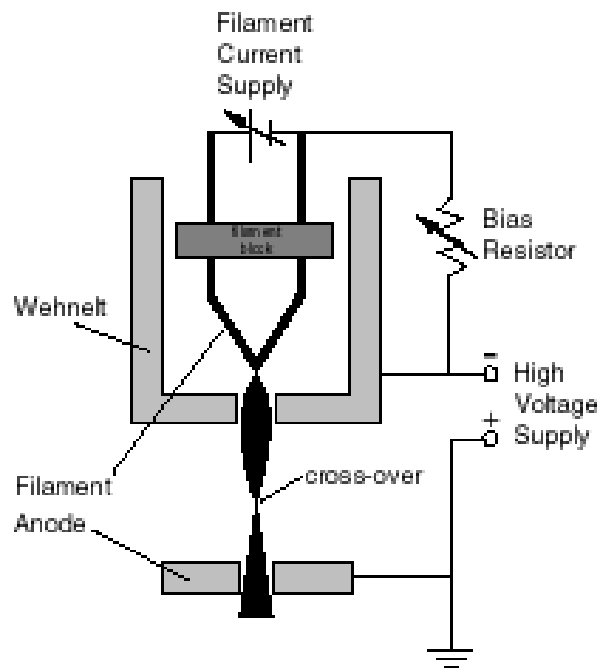


- Vacuum Vessel
- Magnetic Shield
- LN Shield
- LHe Vessel
- RF Cavity
- Photocathode Stalk
- Vacuum/Beam Pipe
- High TC Solenoid
- RF Tuner
- RF Coupler

<https://www6.slac.stanford.edu/news/2018-04-09-slac-produces-first-electron-beam-superconducting-electron-gun.aspx>

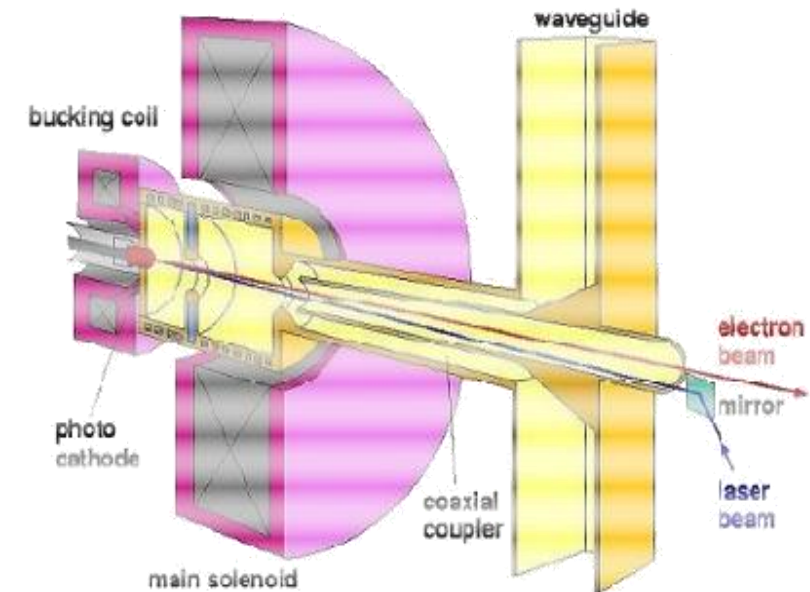


# Components of an electron gun



DC gun for TEM

- Gun type: DC or RF gun
- Main components:
  - A Cathode of some type for generating electrons
  - Accelerating Voltage between the cathode and anode
  - Anode(or not?)
  - Focusing structures
  - Auxiliary system, Vacuum, power, cooling .....



PITZ RF gun for XFEL



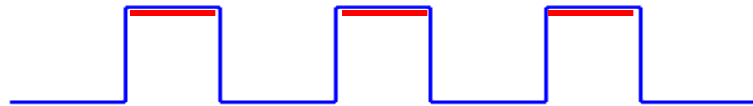
# Typical beam time structures of gun

## DC gun

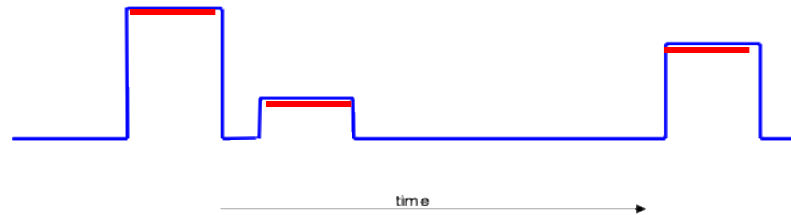
DC always ON



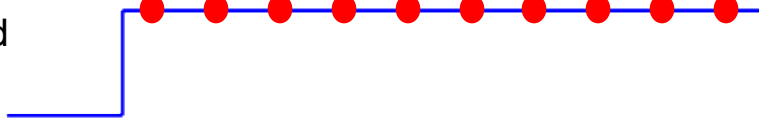
DC Pulsed



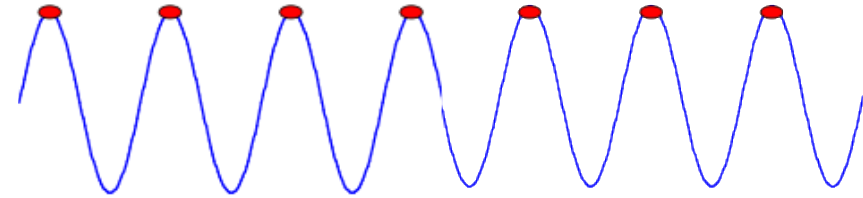
DC Pulsed,  
Amp & Freq  
modulated



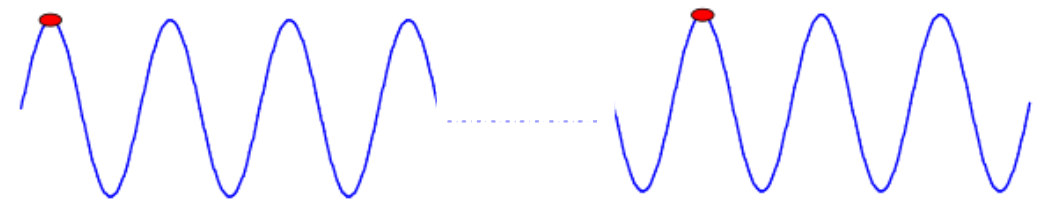
DC always on  
Beam pulsed



## RF gun



CW – bunch of  $e^-$  in every RF bucket, typically from 100's of MHz to GHz, up to 100's of pC per bunch



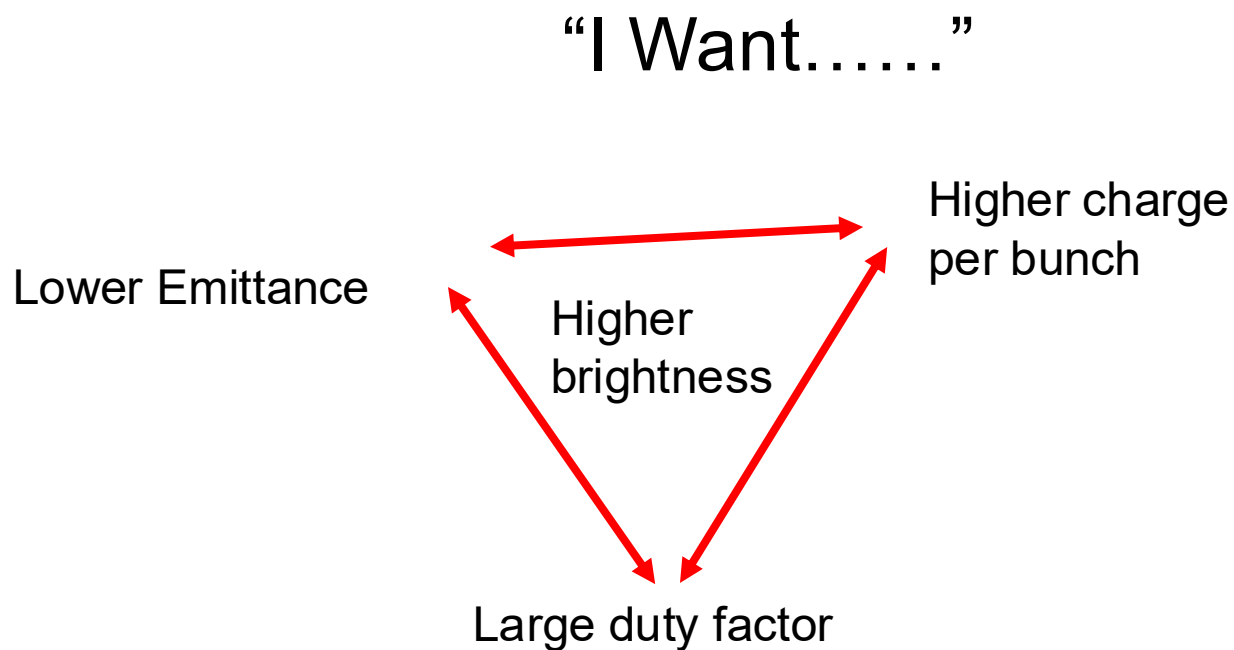
pulsed – not every RF bucket is filled, RF frequencies of 100's of MHz to GHz, up to  $\sim$ nC per bunch, with bunch rep rates of Hz to 1 MHz





# What properties we care about?

- Current (average, peak)
- Bunch charge
- Pulse length
- Beam size
- Emittance
- Beam brightness
- Reliability
- Physical size
- Cost
- .....



No matter what – people always want more than they have!

“Gun determines all”



- Some topics in an electron gun
  - Emittance and phase space
  - Cathode and electron emission
  - Beam emittance in photo-cathode RF gun



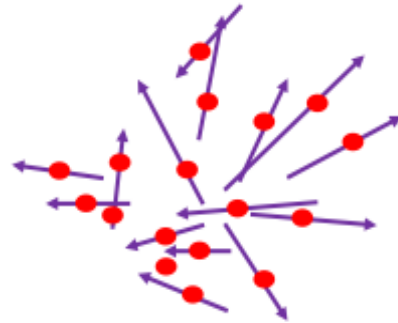


## How good is a Charged Particle Beam?

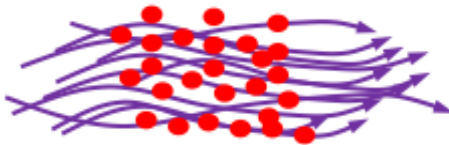
an “ordered flow” of charged particles



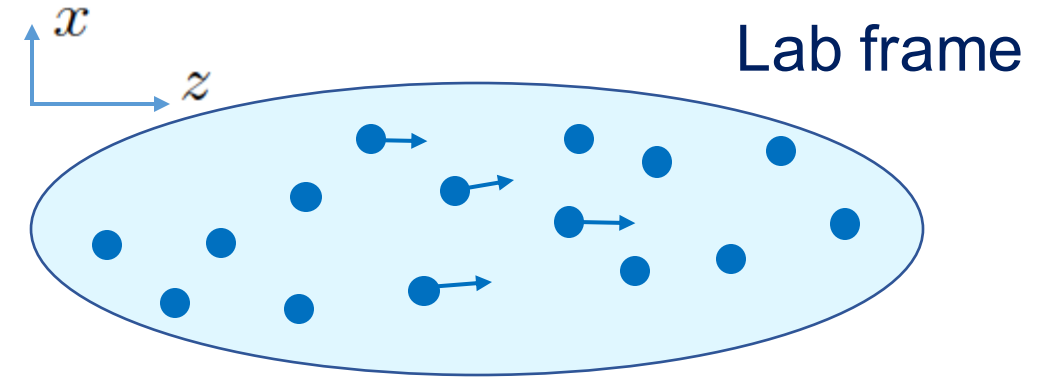
all particles are moving  
along the same trajectory  
for a perfect beam



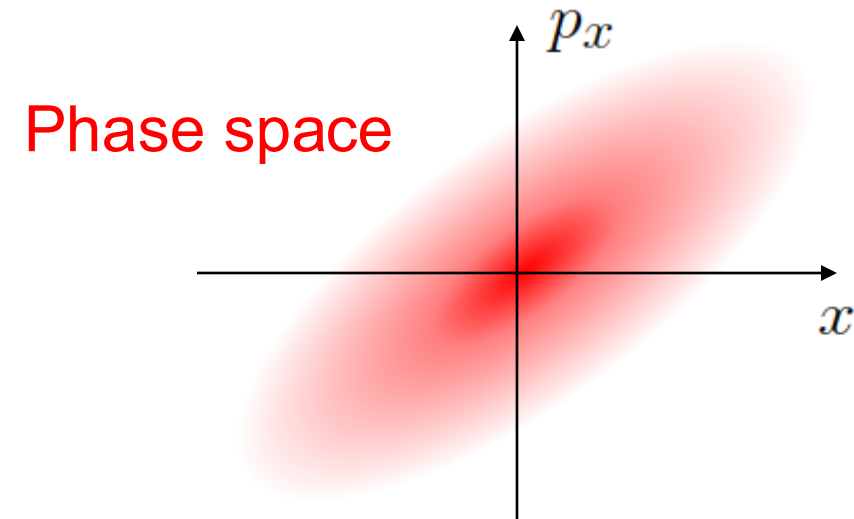
a random distribution  
of charges



something in between  
(real world)



Phase space  $(x, y, z, p_x, p_y, p_z)$  or  $(x, y, t, p_x, p_y, E)$



Emittance (volume)

$$\epsilon_{nx} = \sigma_x \sigma_{p_x}^{14}$$

Emittance is less strictly defined as the area occupied by the a bunch of charged particles in trace space. i.e.

$$\varepsilon_x = A_x = \iint dx dx'. \quad [\pi \text{ m-rad}]$$

The trace-space area  $A_x$  is related to the phase-space area in  $x$ - $p_x$  plane by

$$A_x = \iint dx d\frac{p_x}{p} = \frac{1}{\langle p_z \rangle} \iint dx dp_x = \frac{1}{\gamma\beta} \cdot \frac{1}{mc} \iint dx dp_x \quad p_z \gg p_x$$

It's useful to define 'normalized emittance' that is independent of particle energy such that

$$\varepsilon_n = \gamma\beta\varepsilon$$

But beams with quite different distributions in trace space may occupy the same area!!

Define RMS emittance as

$$\varepsilon_x = \sqrt{\langle x^2 \rangle \langle x'^2 \rangle - \langle xx' \rangle^2} = \sqrt{\sigma_x^2 \sigma_{x'}^2 - \sigma_{xx'}^2} = \sqrt{\det \sigma} \quad \sigma = \begin{bmatrix} \sigma_x^2 & \sigma_{xx'} \\ \sigma_{xx'} & \sigma_{x'}^2 \end{bmatrix}$$

If  $x$  and  $x'$  are not correlated (e.g. at beam waist)

$$\varepsilon_x = \sqrt{\langle x^2 \rangle \langle x'^2 \rangle} = \sigma_x \sigma_{x'}$$

RMS emittance provides a quantitative description of beam quality



## Beam size and beam divergence

root-mean square (RMS) of a set of n values is defined as:

$$x_{rms} = \sqrt{\frac{1}{n} (x_1^2 + x_2^2 + \cdots + x_n^2)}$$

Let  $f(x, x')$  be the distribution function such that  $\int f(x, x') dx dx' = N$ .  $N$  is the total number of particles. Beam parameters can be defined accordingly as:

$$\langle x \rangle = \int x f(x, x') dx dx' / \int f(x, x') dx dx'$$

averaged beam size

$$\langle x' \rangle = \int x' f(x, x') dx dx' / \int f(x, x') dx dx'$$

averaged beam divergence

$$\sigma_x = \sqrt{\int (x - \langle x \rangle)^2 f(x, x') dx dx' / \int f(x, x') dx dx'}$$

rms beam size

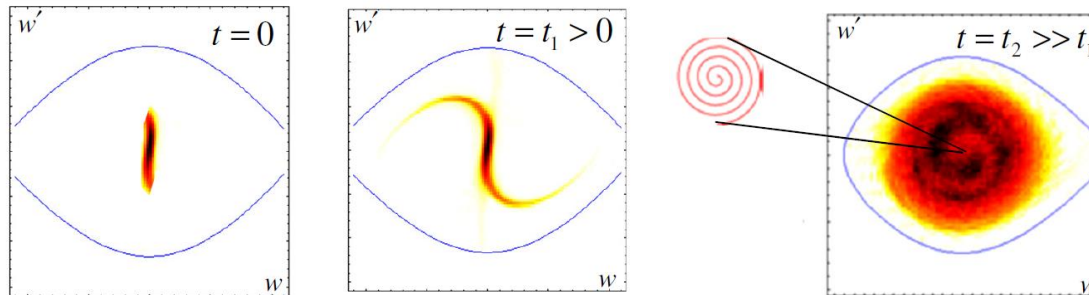
$$\sigma_{x'} = \sqrt{\int (x' - \langle x' \rangle)^2 f(x, x') dx dx' / \int f(x, x') dx dx'}$$

rms beam divergence

$$\sigma_{xx'} = \sqrt{\int (x - \langle x \rangle)(x' - \langle x' \rangle) f(x, x') dx dx' / \int f(x, x') dx dx'}$$

beam correlation

- RMS emittance gives more weight to the particles in the outer region of the trace- space area. Therefore, removing some outer particles will significantly reduce RMS emittance without too much degradation of beam intensity.
- Liouville theorem states that for **Hamiltonian systems the phase space density stays constant**.
- As long as the particle dynamics in the beamline elements (transport optics, accelerating sections) can be described by Hamiltonian functions (no binary collisions, stochastic processes, etc. ), the phase space density will stay constant throughout the accelerator.
- **The phase space density obtained at the electron source is a critical parameter.**
- **In real machines, rms emittances are conserved only when linear forces act on the distribution**



M. Reiser, Theory and Design of Charged Particle Beams (2008)

- Beam brightness(density) is simply defined as

$$\mathcal{B} = \frac{N}{\epsilon_{nx} \cdot \epsilon_{ny} \cdot \epsilon_{nz}}$$



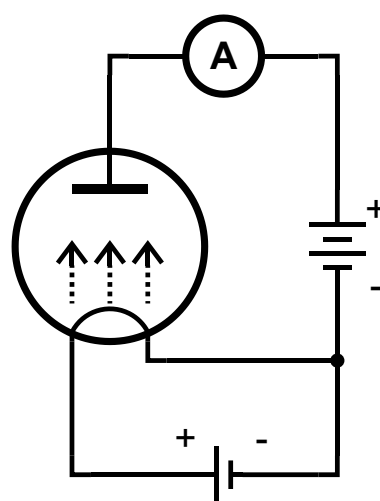
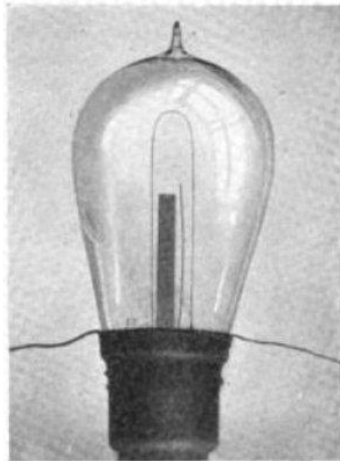
- Some topics in an electron gun
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- Cathode and electron emission
  - Beam emittance in photo-cathode RF gun



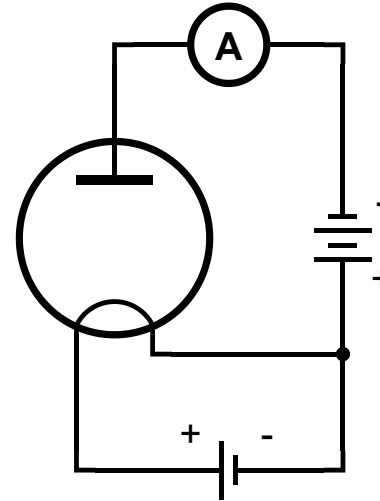


# How to generate free electrons?

- Charging by friction, voltaic battery
- Cathode Ray, Crookes tube
- Guthrie measured the discharge of a positively charged, red-hot sphere into air, helping establish understanding of the thermionic emission phenomenon(1873)
- Edison's work with the light bulb

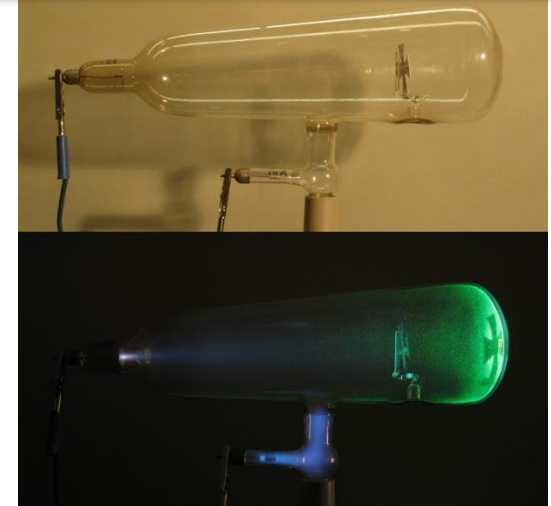


Electron flow



No current

## Crookes-Hittorf tube

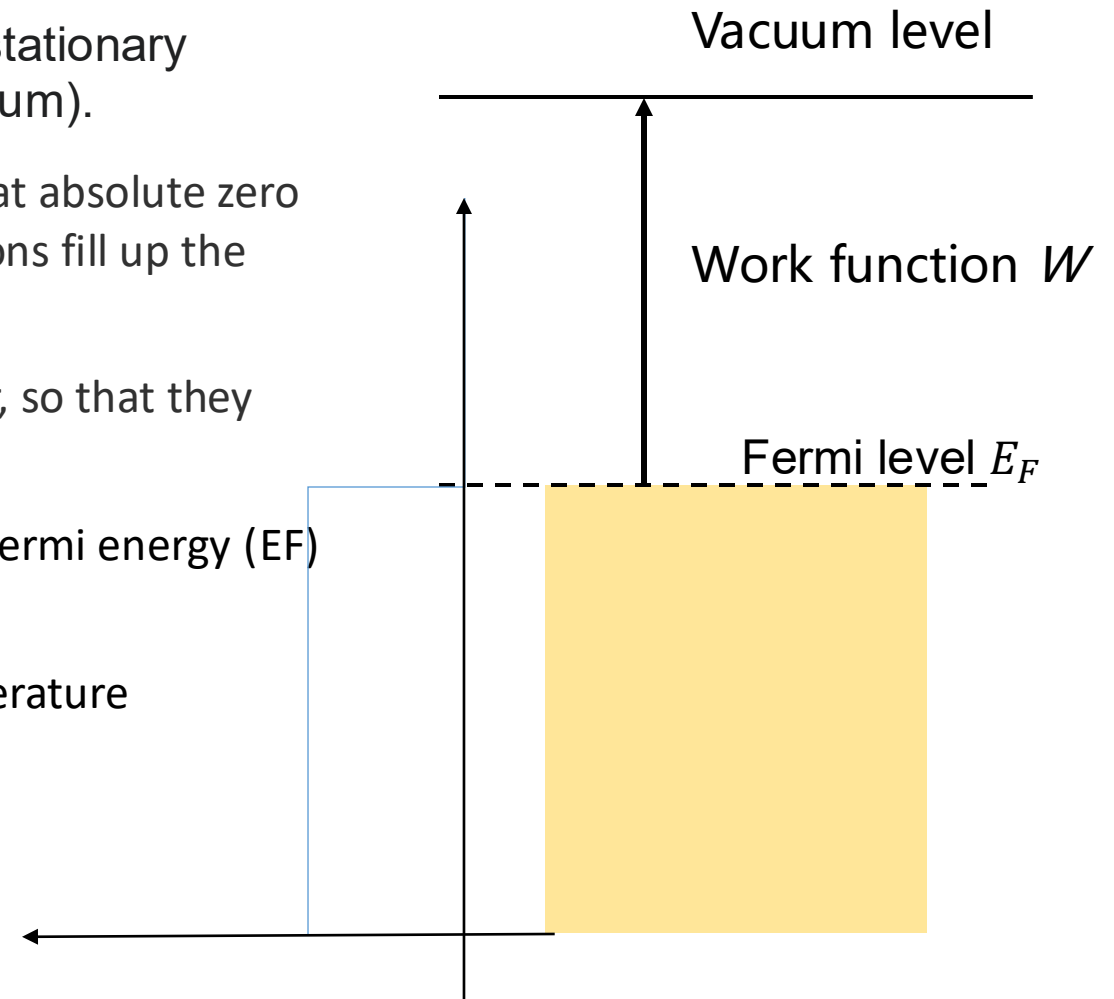




# How to generate free electrons?

- In physics, the **vacuum level** refers to the energy of a free stationary electron that is outside of any material (it is in a perfect vacuum).
- Fermi level: the highest energy level that an electron can occupy at absolute zero temperature. At absolute zero temperature (0 Kelvin), the electrons fill up the energy levels starting from the lowest.
- Give electrons enough energies to overcome the potential barrier, so that they escape from material into vacuum
- Work function, the energy that an electron must gain above the Fermi energy ( $E_F$ ) in order to emit into vacuum,  $W = \text{vacuum level} - \text{Fermi level}$
- Work function depends on cathode material and operation temperature

Ag	4.26 – 4.74	Al	4.06 – 4.26	As	3.75
Au	5.10 – 5.47	B	~4.45	Ba	2.52 – 2.70
Be	4.98	Bi	4.31	C	~5
Ca	2.87	Cd	4.08	Ce	2.9
Co	5	Cr	4.5	Cs	1.95
Cu	4.53 – 5.10	Eu	2.5	Fe:	4.67 – 4.81





# Type of electron emission

- Give the conduction band electrons extra energy:
  - thermionic emission,
  - photoemission,
  - secondary emission
- Change the potential barrier:
  - field emission,
  - plasma emission

***Give electrons enough energies to overcome the potential barrier, so that they escape from material into vacuum***



- The Fermi level ( $E_F$ ) can be defined from the Fermi-Dirac distribution, which is:

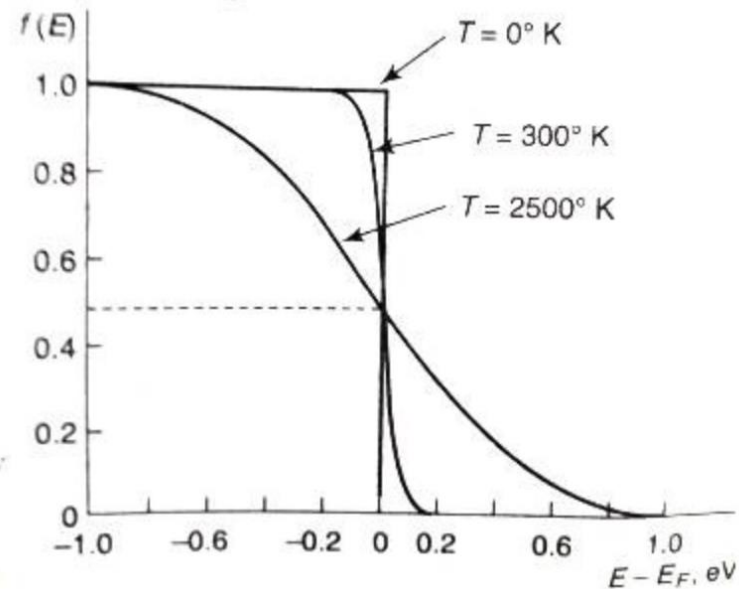
$$f_{FD}(E) = \frac{1}{e^{(E-E_F)/kT} + 1}$$

- Where:

- $f(E)$  is the Fermi-Dirac distribution function, representing the probability of finding an electron with energy state  $E$ .
- $E$  is the energy of the electron
- $E_F$  is the Fermi level
- $k_B$  is Boltzmann's constant,  $k=1.380649 \times 10^{-23}$  J/K,
- $T$  is the temperature in Kelvin

Heaviside-step function,  $H(x)$  when  $T \rightarrow 0$

$$E_f = \frac{h^2}{8m} \left( \frac{3n}{2} \right)^{2/3} \quad n = N/V \text{ is the electron density}$$



Element	Fermi Energy [eV]
Cu	7.00
Mg	7.08
Ba	3.64
Pb	9.47



# Density of available states in metal

- Electron motion in the conduction band can be approx. modeled by free particles bound by infinite potential barriers located at the physical boundaries of the metal
- Solving the time independent Schrodinger equation under these boundary conditions, **Born-Karman boundary conditions**
- The corresponding wave functions are:

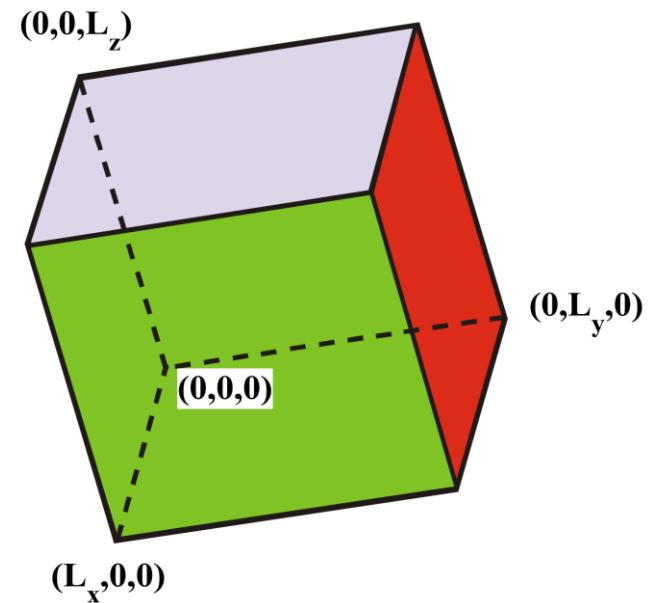
$$\Psi(x, y, z) = \sin(k_x x) \sin(k_y y) \sin(k_z z)$$

- Where:

$$k_x L_x = 2\pi n_x, k_y L_y = 2\pi n_y, k_z L_z = 2\pi n_z$$

$$n_i = 1, 2, 3, 4 \dots \dots \infty,$$

$$E(k) = \frac{\hbar^2 k^2}{2m} = \frac{\hbar^2}{2m} (k_x^2 + k_y^2 + k_z^2) \quad E = \frac{p^2}{2m} = \frac{1}{2} m v^2$$







# Density of available states in metal

- Density of state in k-space:

$$\frac{k_x k_y k_z}{n_x n_y n_z} = \Delta \tilde{k} = \left(\frac{2\pi}{L_x}\right) \cdot \left(\frac{2\pi}{L_y}\right) \cdot \left(\frac{2\pi}{L_z}\right) = \frac{(2\pi)^3}{V}$$

$$\rho(k) = \frac{1}{\Delta \tilde{k}} = \frac{V}{8\pi^3}$$

- Total number of k value in k-space:  $\rho(\mathbf{k}) \cdot \frac{4}{3}\pi k^3$

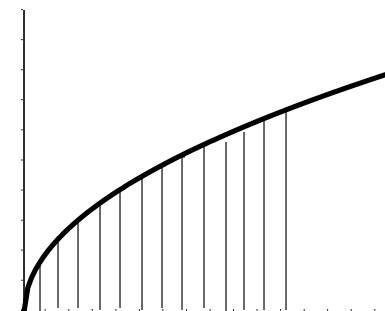
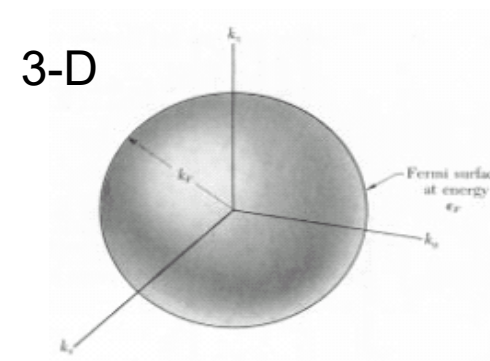
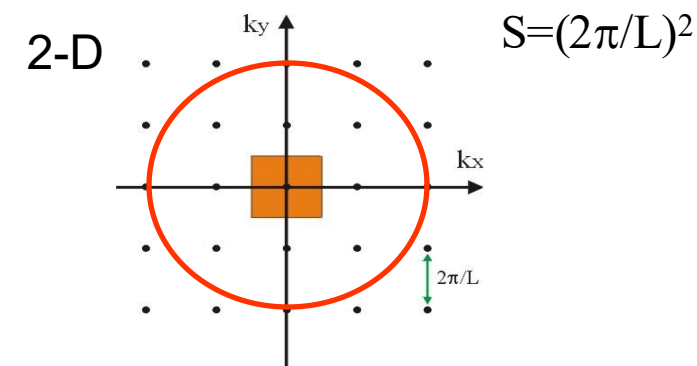
- Total number of energy state:

Electron is fermion, Pauli exclusion principle, different spin

$$Z(E) = 2 \cdot \rho(k) \cdot \frac{4}{3}\pi k^3 = 2 \cdot \frac{V}{8\pi^3} \cdot \frac{4}{3}\pi \frac{(2m)^{\frac{3}{2}}}{\hbar^3} E^{\frac{3}{2}} = \frac{V(2m)^{\frac{3}{2}}}{3\pi^2 \hbar^3} \cdot E^{\frac{3}{2}} = N$$

- Density of state per unit volume per unit energy interval

$$n(E) = \frac{d \frac{Z(E)}{V}}{dE} = \frac{(2m)^{\frac{3}{2}}}{2\pi^2 \hbar^3} \cdot E^{\frac{1}{2}} = \frac{8\sqrt{2}\pi m^{\frac{3}{2}}}{h^3} E^{\frac{1}{2}}$$





- Fermi-Dirac distribution function

$$f_{FD}(E) = \frac{1}{e^{(E-E_F)/kT} + 1}$$

- Density of electrons per unit energy interval

$$n(E)dE = \frac{8\sqrt{2}\pi m^{\frac{3}{2}}}{h^3} E^{\frac{1}{2}} \frac{1}{e^{(E-E_F)/kT} + 1}$$

- Number of state in p or k or v space

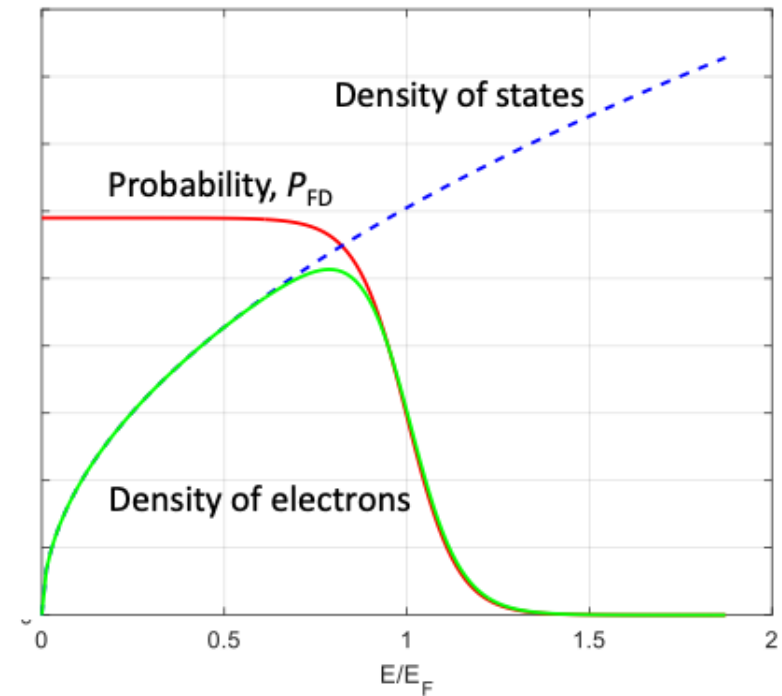
$$dS = 2V dk_x dk_y dk_z / (2\pi)^3 \quad \Delta \tilde{k} = \left(\frac{2\pi}{L_x}\right) \cdot \left(\frac{2\pi}{L_y}\right) \cdot \left(\frac{2\pi}{L_z}\right) = \frac{(2\pi)^3}{V}$$

$$k = \frac{2\pi}{\lambda} = \frac{2\pi p}{h}$$

$$dS = \frac{2V}{h^3} dp_x dp_y dp_z$$

$$E = \frac{p^2}{2m} = \frac{1}{2} m v^2$$

- Where  $p_x = m v_x \Rightarrow dp_x = m dv_x$ , so  $dS = \frac{2V}{h^3} \cdot m^3 dv_x dv_y dv_z$





- Some electrons can reach energy greater than fermi level and vacuum level and escape to vacuum when the temperature  $T$  is high enough.
- The number of electrons in velocity space  $v_x \rightarrow (v_x + dv_x)$ ,  $v_y \rightarrow (v_y + dv_y)$ ,  $v_z \rightarrow (v_z + dv_z)$  is

$$dN = f(E) \cdot dS = \frac{1}{e^{(E-E_F)/kT} + 1} \frac{2V}{h^3} \cdot m^3 dv_x dv_y dv_z \quad \text{and the density: } dn = \frac{dN}{V}$$

- For thermionic emission,  $E - E_F \gg kT$ , then

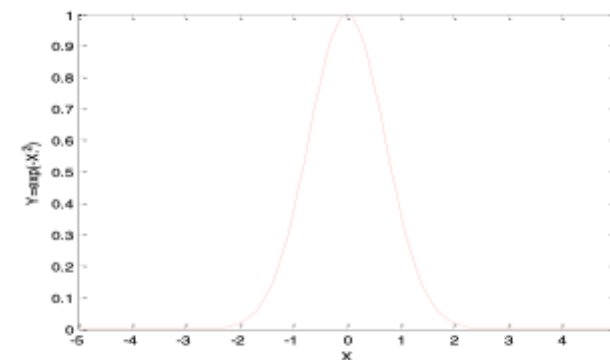
$$f_{FD}(E) \approx e^{-(E-E_F)/kT} = e^{\frac{E_F}{kT}} \cdot e^{-\frac{1}{kT} \cdot \frac{1}{2} m (v_x^2 + v_y^2 + v_z^2)}$$

$$dn = \frac{dN}{V} = \frac{2m^3}{h^3} e^{\frac{E_F}{kT}} \cdot e^{-\frac{m}{2kT} v_x^2} dv_x \cdot e^{-\frac{m}{2kT} v_y^2} dv_y \cdot e^{-\frac{m}{2kT} v_z^2} dv_z$$

- The density of current:

$$dJ = e v_z dn = e v_z \frac{2m^3}{h^3} e^{\frac{E_F}{kT}} \cdot e^{-\frac{m}{2kT} v_x^2} dv_x \cdot e^{-\frac{m}{2kT} v_y^2} dv_y \cdot e^{-\frac{m}{2kT} v_z^2} dv_z$$

Maxwellian velocity distribution



$z$  is direction of emission,  
normal to cathode surface.



# Richardson-Dushman equation

- Only electrons with energy greater than  $E_F + W$  and with velocity  $v_z$  in z-direction larger than the critical velocity  $v_{z0}$  contribute to thermionic emission, so the current is

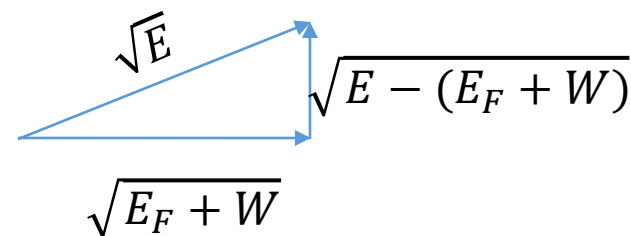
$$J = \int dJ = \frac{2em^3}{h^3} e^{\frac{E_F}{kT}} \int_{-\infty}^{+\infty} e^{-\frac{m}{2kT}v_x^2} dv_x \int_{-\infty}^{+\infty} e^{-\frac{m}{2kT}v_y^2} dv_y \int_{v_{z0}}^{+\infty} v_z e^{-\frac{m}{2kT}v_z^2} dv_z$$

$$\frac{1}{2}mv_z^2 \geq E_F + W,$$

$$v_{z0} = \sqrt{\frac{2(E_F + W)}{m}}$$

$$\int_{-\infty}^{+\infty} e^{-ax^2} dx = \sqrt{\pi/a}, \text{ so } \int_{-\infty}^{+\infty} e^{-\frac{m}{2kT}v_x^2} dv_x = \sqrt{\frac{2\pi kT}{m}}$$

$$\int xe^{-ax^2} dx = -\frac{e^{-ax^2}}{2a}, \text{ so } \int_{v_{z0}}^{+\infty} v_z e^{-\frac{m}{2kT}v_z^2} dv_z = \frac{kT}{m} e^{-\frac{E_F+W}{kT}}$$



$$J = \frac{2em^3}{h^3} e^{\frac{E_F}{kT}} \cdot \frac{2\pi kT}{m} \cdot \frac{kT}{m} e^{-\frac{E_F+W}{kT}} = \frac{4\pi emk^2}{h^3} T^2 e^{-\frac{W}{kT}} = A T^2 e^{-\frac{W}{kT}}$$

Richardson-Dushman equation :

$$J_{th} = A T^2 e^{-\frac{W}{kT}}$$

$$A = \frac{4\pi emk^2}{h^3} = 1.202 \times 10^6 \text{ A m}^{-2}\text{K}^{-2}$$

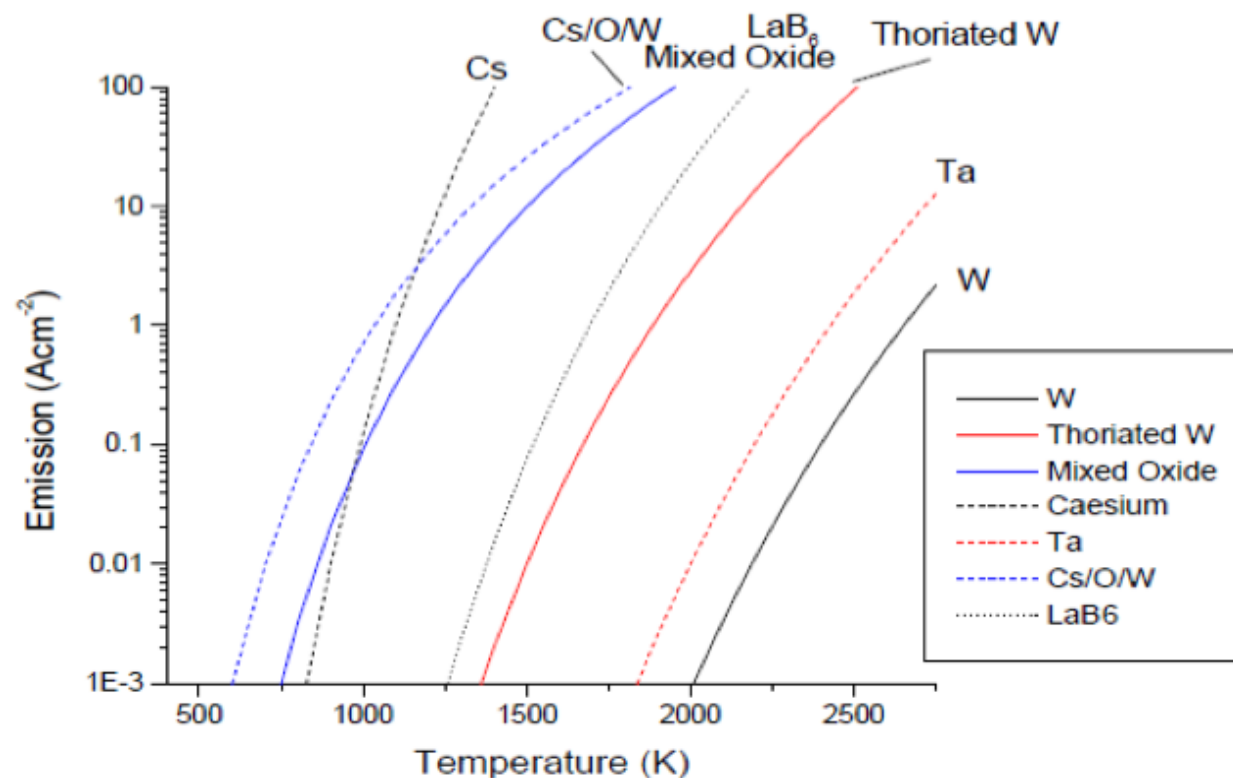


# Richardson-Dushman equation

- Work function and Richardson constant of various materials

- Thermionic emission of various cathode materials

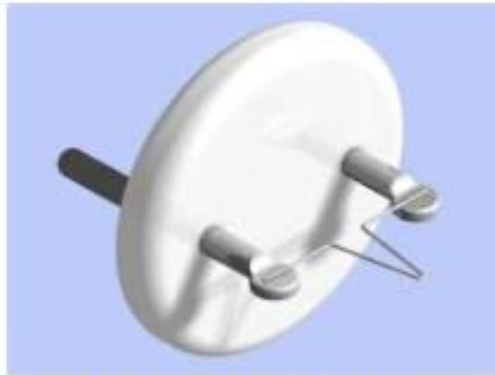
Material	W (eV)	$A^*b$ ( $A\ cm^{-2}\ K^{-2}$ ) (b is material correction factor)
Molybdenum	4.15	55
Nickel	4.61	30
Tantalum	4.12	60
Tungsten	4.54	60
Barium	2.11	60
Cesium	1.81	160
Iridium	5.40	170
Platinum	5.32	32
Rhenium	4.85	100
Thorium	3.38	70
Ba on W	1.56	1.5
Cs on W	1.36	3.2
Th on W	2.63	3.0
Thoria	2.54	3.0
BaO + SrO	0.95	$\sim 10^{-2}$
Cs-oxide	0.75	$\sim 10^{-2}$
TaC	3.14	0.3
LaB <sub>6</sub>	2.70	29
theoretical:		120.2 (b=1)



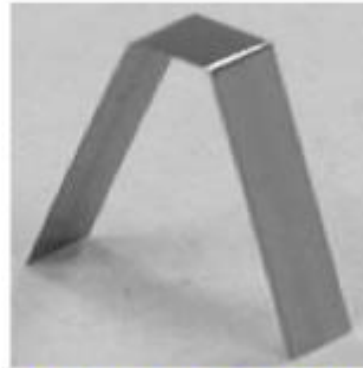




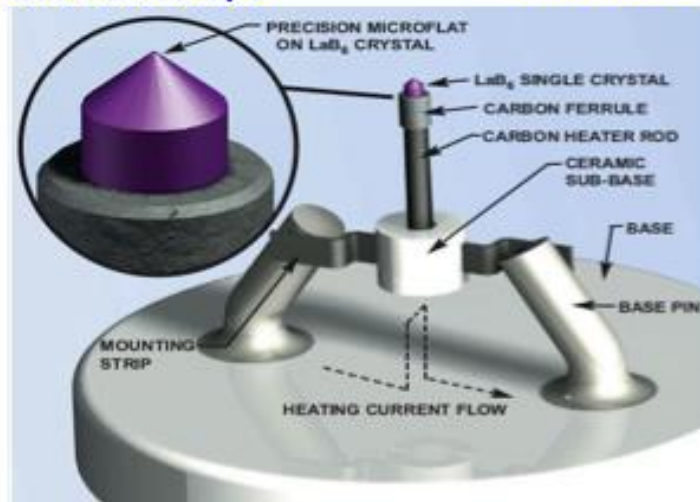
# Common thermionic cathodes



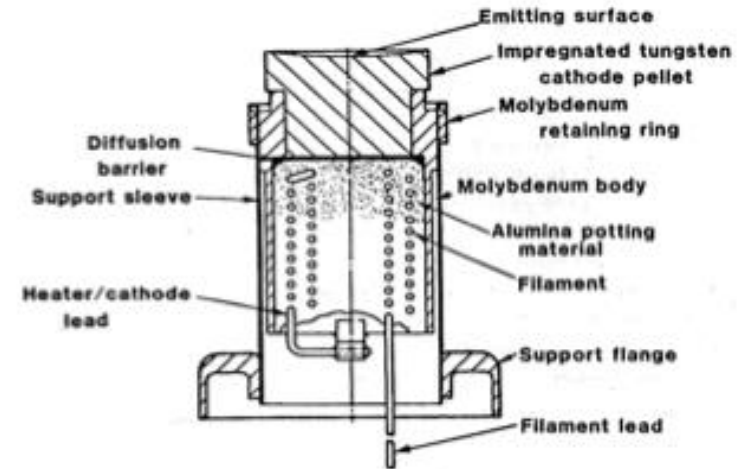
tungsten filament for  
electron microscope



filament cathode for  
e-beam welder



LaB<sub>6</sub> cathode for  
electron microscope



a typical type B dispenser cathode for linac system



# Planar diode with space charge – Child-Langmuir Law

$$\begin{cases} \nabla^2 \phi = \frac{d^2 \phi}{dx^2} = -\frac{\rho}{\epsilon_0} \\ J_x = \rho \dot{x} = \text{const} \\ \frac{m}{2} \dot{x}^2 - e\phi(x) = 0 \end{cases}$$

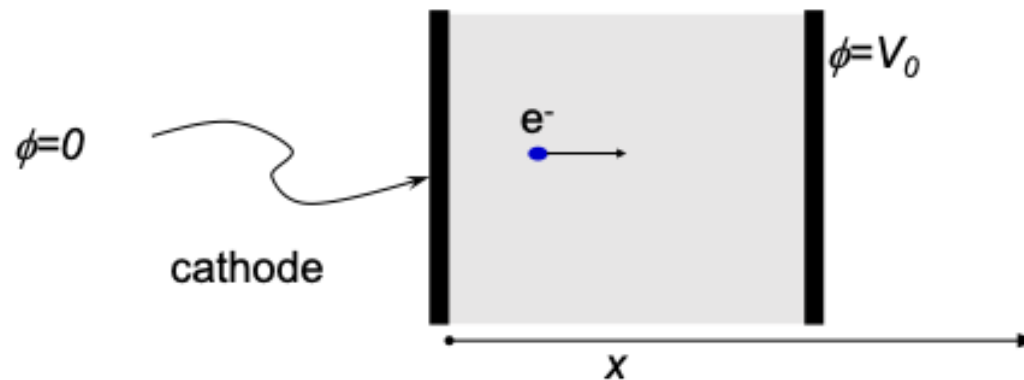
$$\Rightarrow \frac{d^2 \phi}{dx^2} = \frac{J}{\epsilon_0 (2e/m)^{1/2}} \frac{1}{(\phi)^{1/2}}$$

$$\Rightarrow \left( \frac{d\phi}{dx} \right)^2 = \frac{4J}{\epsilon_0 (2e/m)^{1/2}} \phi^{1/2} + C$$

$$\Rightarrow \frac{4}{3} \phi^{3/4} = 2 \left( \frac{J}{\epsilon_0} \right)^{1/2} \left( \frac{2e}{m} \right)^{-1/4} x$$

$$\Rightarrow \phi(x) = V_0 \left( \frac{x}{d} \right)^{4/3} \quad \text{with} \quad J = \frac{4}{9} \epsilon_0 \left( \frac{2e}{m} \right)^{1/2} \frac{V_0^{3/2}}{d^2}$$

**Child-Langmuir law**



$C=0$  under the boundary conditions:  $\phi=0$  and  $d\phi/dx=0$  at  $x=0$ ; the condition  $d\phi/dx=0$  at  $x=0$  implies that the special case **electric field at cathode surface is null** (a steady state solution).

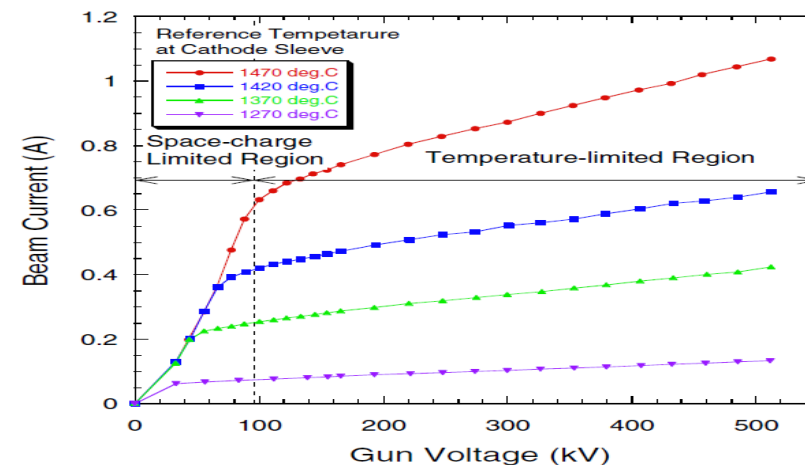




Image charge force:

$$eE_I(x) = \frac{-e^2}{4\pi\epsilon_0(2x)^2}$$

Image charge potential:

$$\phi_I(x) = -\int_x^\infty E_I(x)dx = \frac{e}{16\pi\epsilon_0 x}$$

With applied field potential:

$$\phi(x) = -eE_a x - \frac{e^2}{16\pi\epsilon_0 x}$$

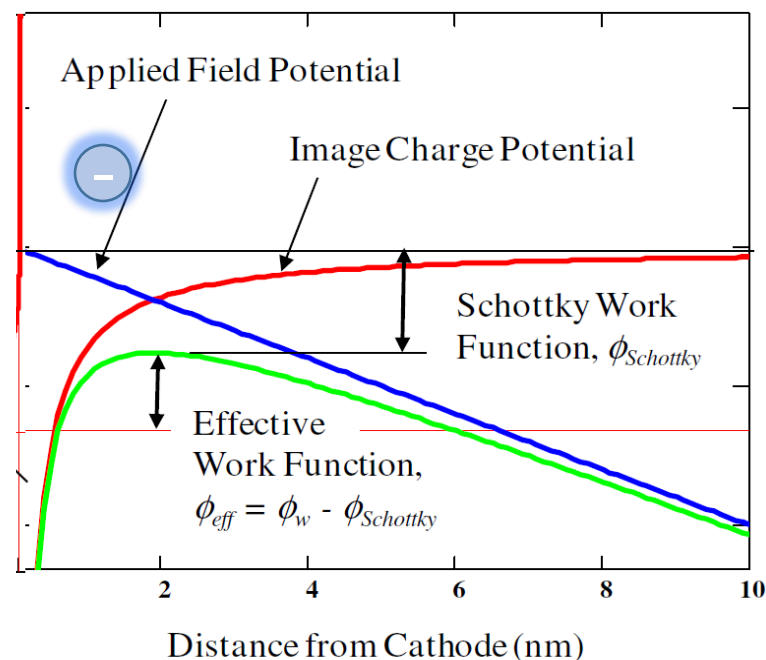
$$\frac{d\phi}{dx} = -eE_a + \frac{e^2}{16\pi\epsilon_0 x^2} = 0 \Rightarrow x_m = \sqrt{\frac{e}{16\pi\epsilon_0 E_a}}$$

Maximum of potential:

$$\phi_m = -W = -e \sqrt{\frac{eE_a}{4\pi\epsilon_0}}$$

Effective work function:  $\phi_{eff} = \phi_w - \phi_{schottky}$

$$J_e = A T^2 e^{-\frac{W-\Delta W}{kT}} = J_{th} \text{Exp}\left(\frac{e(eE/4\pi\epsilon_0)^{\frac{1}{2}}}{kT}\right)$$



$$\Delta W = e \sqrt{\frac{eE_a}{4\pi\epsilon_0}}$$

Schottky barrier lowering

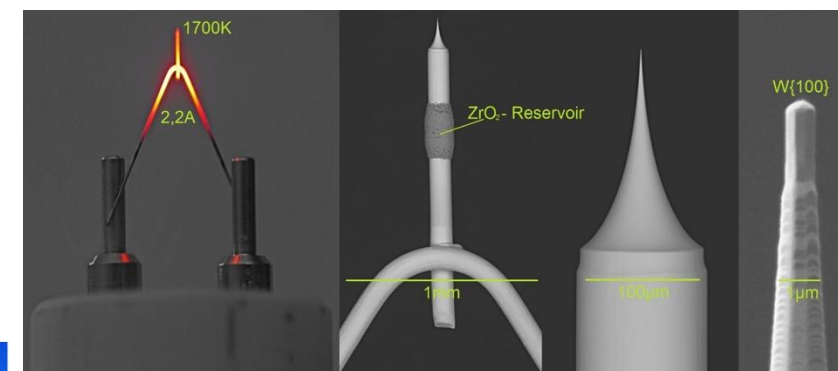
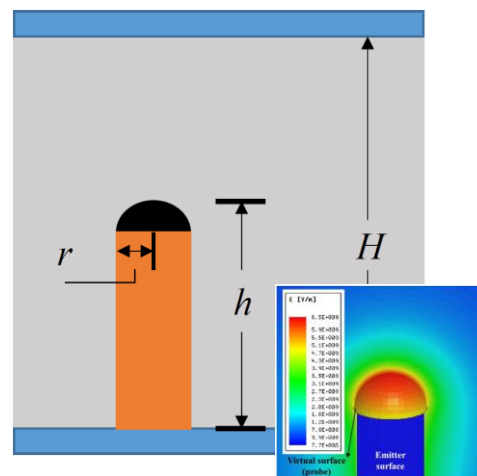
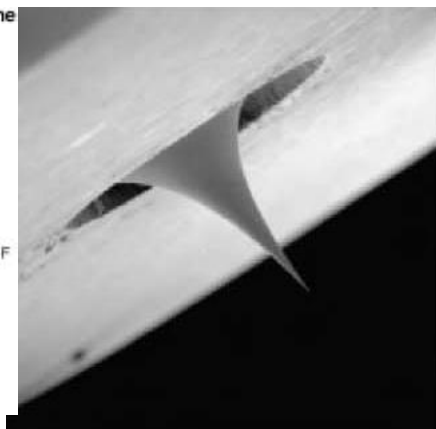
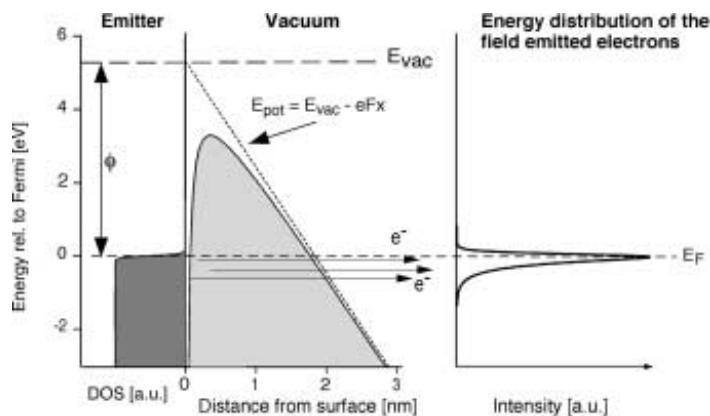


- When the electric field at the surface of a cathode reaches a critical level, the diode current is observed to rise sharply.
- The potential barrier is suppressed and distorted by applied field, and electron can “tunnel” through the barrier. The barrier penetration depends on the work function, the Fermi level, and the field strength.
- The emission current density is given by the Fowler-Nordheim equation, the current density is extremely sensitive function of the field.
- The required field are quite high ( $10^7$ - $10^8$  V/m), significant field enhancement occurs on the tip.
- The source of dark current in a gun

$$J_{FN}(F) = A_{FN} E^2 \exp\left(-\frac{B_{FN} W^{3/2}}{E}\right)$$

$$E_{\text{apex}} = \beta E_M = \beta \frac{V}{H}$$

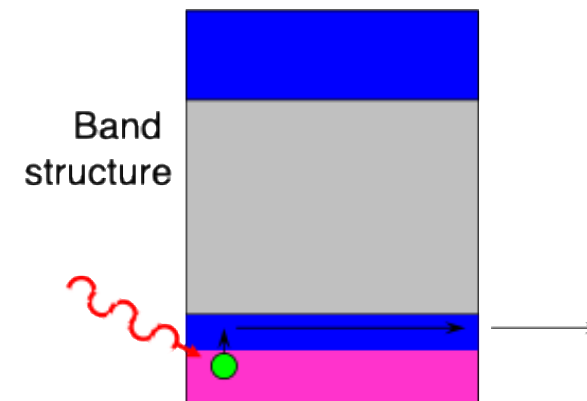
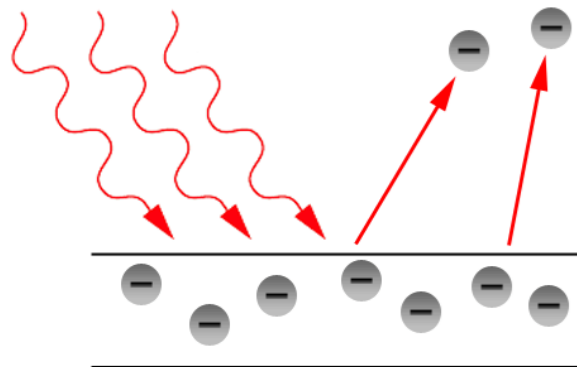
$\beta$ : field enhancement factor



Thermionic and cold field emission

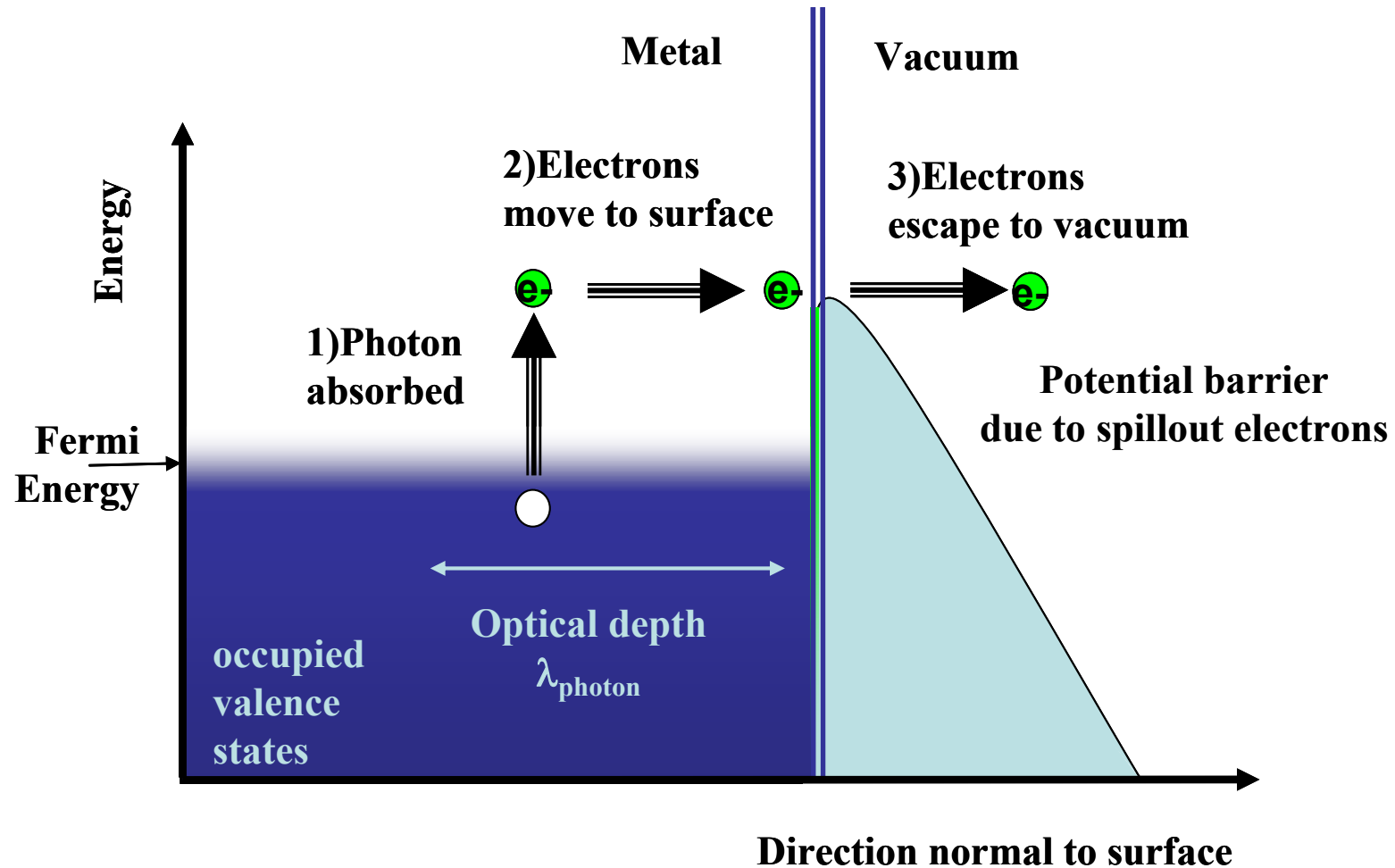


- Electron produced by shining light on surface of metal
  - Below the threshold energy(wavelength) no electrons are emitted
  - Above the threshold, electron energy is the same at any wavelength of light independent of intensity
- Einstein proposed that this is due to the particle nature of light, predicted energy dependence of electrons on incident light wavelength ( Nobel prize for work on the photoelectric effect)
- Type of photocathodes:
  - Metals: copper, Mg; low efficiency, good time response, resistant to contamination, UV laser
  - Semi-conductors: GaAs, Cs<sub>2</sub>Te, K<sub>2</sub>CsSb, GaN; high efficiency, slower time response, sensitive to contamination, visible/IR/UV laser





- 3-step model (excite, transport, escape) used to explain the emission process



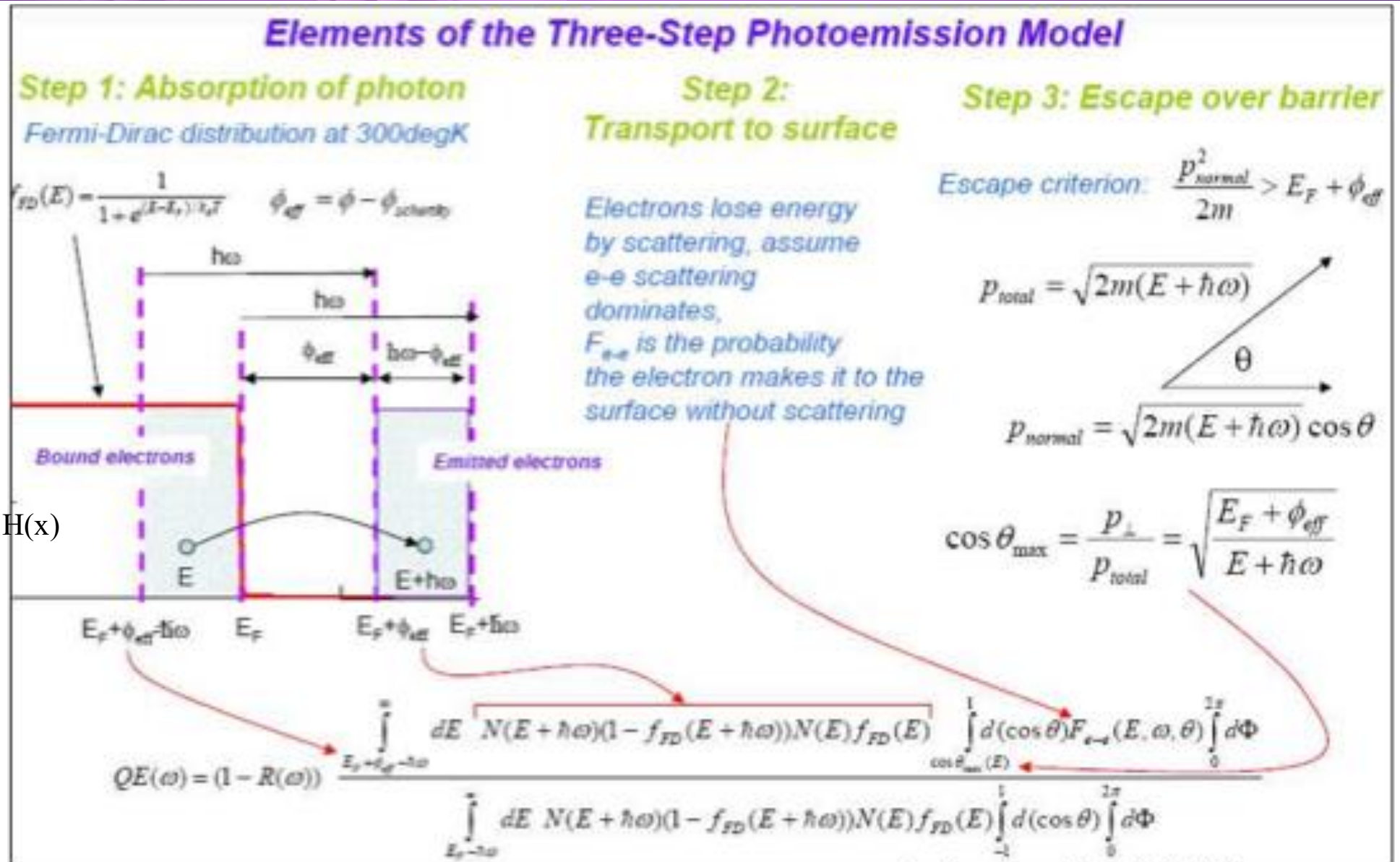


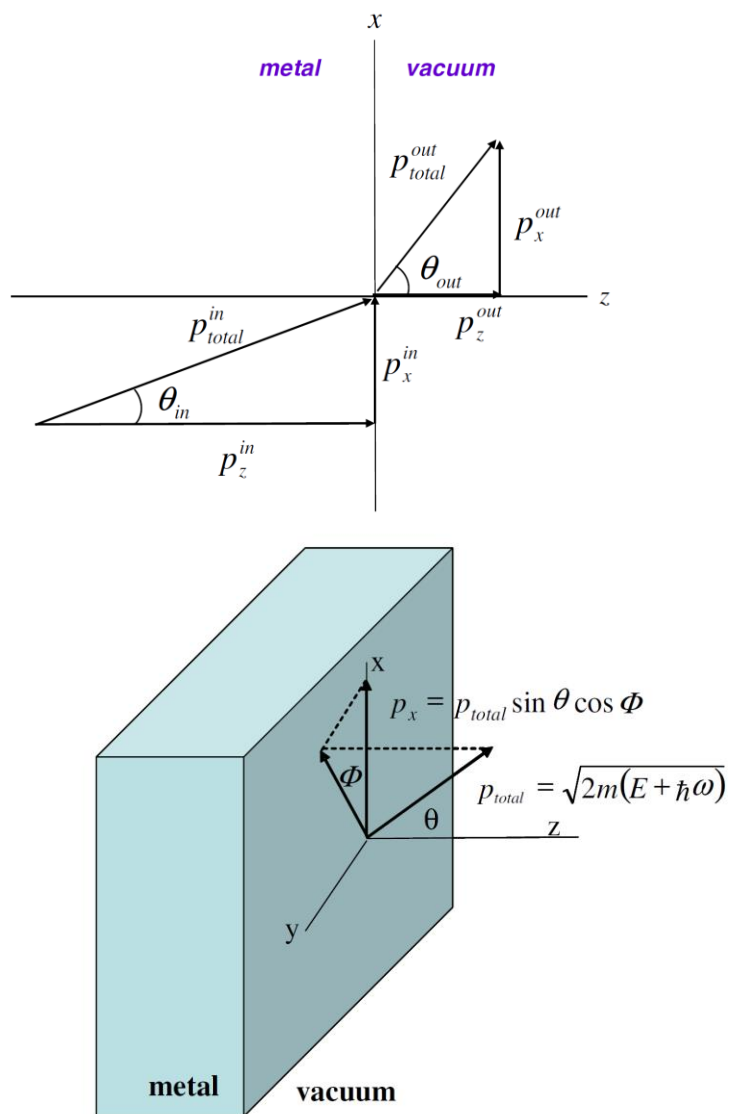
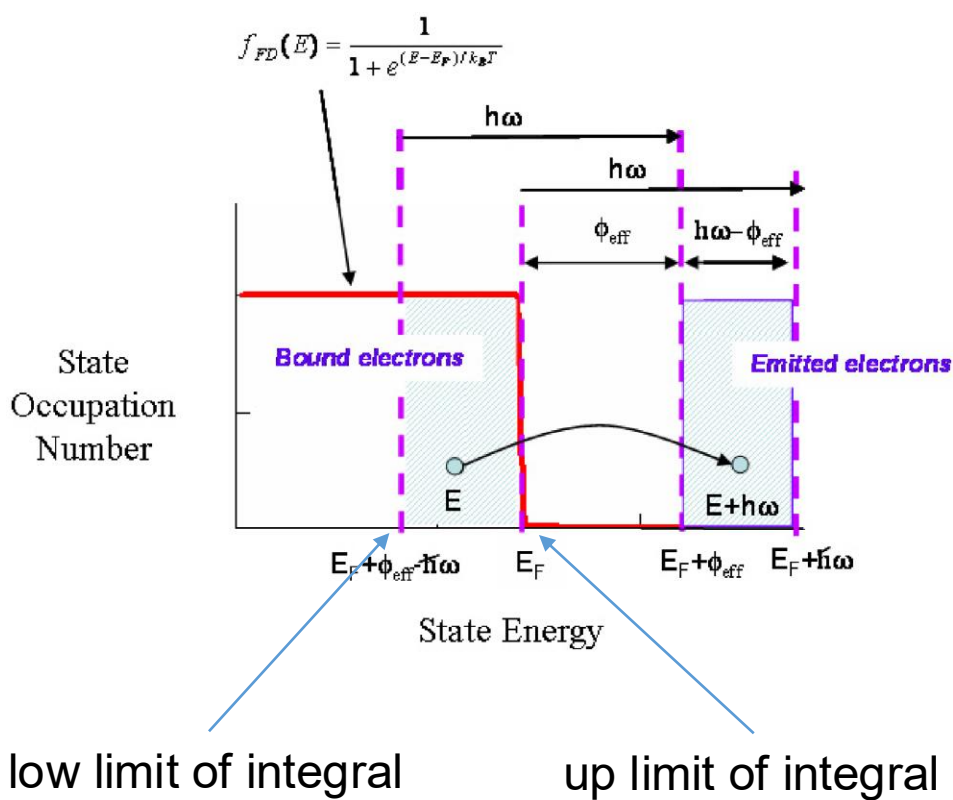


$$QE = \frac{N_e}{N_{ph}}$$

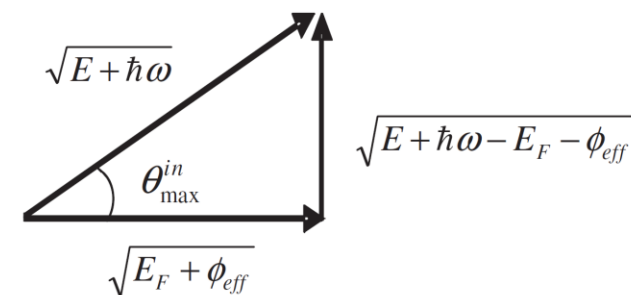
Heaviside-step function,  $H(x)$

$$kT \ll \hbar\omega$$





$$\cos \theta_{\text{max}}^{\text{in}} = \sqrt{\frac{E_F + \phi_{\text{eff}}}{E + \hbar\omega}}$$





$$QE(\omega) = [1 - R(\omega)] \frac{\int_{E_F + \phi_{eff} - \hbar\omega}^{\infty} dE [1 - f_{FD}(E + \hbar\omega)] f_{FD}(E) \int_{\cos\theta_{\max}(E)}^1 d(\cos\theta) F_{e-e}(E, \omega, \theta) \int_0^{2\pi} d\Phi}{\int_{E_F - \hbar\omega}^{\infty} dE [1 - f_{FD}(E + \hbar\omega)] f_{FD}(E) \int_{-1}^1 d(\cos\theta) \int_0^{2\pi} d\Phi}$$

$$QE(\omega) = \frac{1 - R(\omega)}{1 + \frac{\lambda_{opt}(\omega)}{\bar{\lambda}_{e-e}(\omega)}} \frac{(E_F + \phi_{eff})}{2\hbar\omega} \left[ 1 - \sqrt{\frac{E_F + \phi_{eff}}{E_F + \hbar\omega}} \right]^2$$

$$QE(\omega) = QE \Big|_{\hbar\omega = \phi_{eff}} + \frac{dQE}{d\hbar\omega} \Big|_{\hbar\omega = \phi_{eff}} (\hbar\omega - \phi_{eff}) + \frac{1}{2} \frac{d^2 QE}{d\hbar\omega^2} \Big|_{\hbar\omega = \phi_{eff}} (\hbar\omega - \phi_{eff})^2 + \dots$$

$$QE(\omega) \approx \frac{1 - R(\omega)}{1 + \frac{\lambda_{opt}(\omega)}{\bar{\lambda}_{e-e}(\omega)}} \frac{(\hbar\omega - \phi_{eff})^2}{8\phi_{eff}(E_F + \phi_{eff})}$$

$$\begin{aligned} F_{e-e}(\omega) &= \int_0^{\infty} f(s, \theta = 0, \omega) ds \\ &= \int_0^{\infty} \frac{1}{\lambda_{opt}(\omega)} e^{-s\{[1/\lambda_{opt}(\omega)] + (1/\bar{\lambda}_{e-e})\}} ds \\ &= \frac{1}{1 + \frac{\lambda_{opt}(\omega)}{\bar{\lambda}_{e-e}}} \end{aligned}$$

$$\bar{\lambda}_{e-e}(\omega) = \frac{\int_{\phi_{eff}}^{\hbar\omega} \lambda_{e-e}(E) dE}{\int_{\phi_{eff}}^{\hbar\omega} dE} = \frac{2\lambda_m E_m^{3/2}}{\hbar\omega \sqrt{\phi_{eff}}} \frac{1}{(1 + \sqrt{\frac{\phi_{eff}}{\hbar\omega}})}$$

More details: An Engineering Guide to Photoinjectors



# transverse emittance in the three-step mode

$$\varepsilon_x = \sqrt{\langle x^2 \rangle \langle x'^2 \rangle - \langle xx' \rangle^2} = \sqrt{\sigma_x^2 \sigma_{x'}^2 - \sigma_{xx'}^2} = \sigma_x \sigma_{x'}$$

$$\varepsilon_{xn} = \beta \gamma \varepsilon_x = \frac{1}{mc} \sqrt{\langle x^2 \rangle} \sqrt{\langle p_x^2 \rangle} = \sigma_x \sigma_{p_x}$$

$$\sigma_{p_x} \equiv \frac{\sqrt{\langle p_x^2 \rangle}}{mc}$$

the dimensionless rms transverse momentum

$$\sigma_{p_x}^2 = \frac{\int_{E_F + \phi_{\text{eff}} - \hbar\omega}^{\infty} dE [1 - f_{\text{FD}}(E + \hbar\omega)] f_{\text{FD}}(E) \int_{\cos\theta_{\text{max}}(E)}^1 d(\cos\theta) \int_0^{2\pi} d\Phi p_x^2 \int_0^{\infty} ds f(s, E, \theta, \omega)}{(mc)^2 \int_{E_F + \phi_{\text{eff}} - \hbar\omega}^{\infty} dE [1 - f_{\text{FD}}(E + \hbar\omega)] f_{\text{FD}}(E) \int_{\cos\theta_{\text{max}}(E)}^1 d(\cos\theta) \int_0^{2\pi} d\Phi \int_0^{\infty} ds f(s, E, \theta, \omega)}$$



$$\sigma_{p_x} = \sqrt{\frac{\hbar\omega - \phi_{\text{eff}}}{3mc^2}}$$

The normalized emittance

$$\varepsilon_n = \sigma_x \sigma_{p_x} = \sigma_x \sqrt{\frac{\hbar\omega - \phi_{\text{eff}}}{3mc^2}}$$

Mean Transverse Energy:  $\text{MTE} = \frac{1}{2} m v^2$

$$\text{MTE} = \frac{1}{N} \sum_1^N \frac{p_{x,y}^2}{2m}$$

$$\varepsilon_n = \sigma_x \sigma_{p_x} = \sigma_x \sqrt{\frac{\text{MTE}}{mc^2}}$$





# Widely used (still not fully understood) photocathodes

	Metallic	Semi-conductor
QE	$10^{-5}$ - $10^{-3}$	$>10^{-2}$
$\lambda_{ph}$	UV	UV-IR
$t_{\text{response}}$	$\sim 10$ fs	$>$ sub-ps
Vacuum	$10^{-9}$ torr	$<10^{-10}$ torr
Life time	years	up to months

Metal Cathodes	Wavelength & Energy: $\lambda_{opt}$ (nm), $\hbar\omega$ (eV)	Quantum Efficiency (electrons per photon)	Vacuum for 1000 Hr Operation (Torr)	Work Function, $\phi_w$ (eV)	Thermal Emittance (microns/mm(rms))	
					Theory	Expt.
Bare Metal						
Cu	250, 4.96	$1.4 \times 10^{-4}$	$10^{-9}$	4.6 [34]	0.5	$1.0 \pm 0.1$ [39] $1.2 \pm 0.2$ [40] $0.9 \pm 0.05$ [3]
Mg	266, 4.66	$6.4 \times 10^{-4}$	$10^{-10}$	3.6 [41]	0.8	$0.4 \pm 0.1$ [41]
Pb	250, 4.96	$6.9 \times 10^{-4}$	$10^{-9}$	4.0 [34]	0.8	?
Nb	250, 4.96	$\sim 2 \times 10^{-5}$	$10^{-10}$	4.38 [34]	0.6	?
Coated Metal						
CsBr:Cu	250, 4.96	$7 \times 10^{-3}$	$10^{-9}$	$\sim 2.5$	?	?
CsBr:Nb	250, 4.96	$7 \times 10^{-3}$	$10^{-9}$	$\sim 2.5$	?	?

## Important References:

- D. Dowell et al. *Cathode R&D* for future light sources. NIMA 622:13 (2010)
- Photocathode Physics for Photoinjectors workshop series.

Typical MTE 0.5 eV  $\rightarrow$   $\sim 1$  mrad

## Common cathode materials:

- Metals: Cu, Mg, Au, Pb, ...
- Semiconductors: Cs<sub>2</sub>Te, K<sub>2</sub>CsSb, GaAs

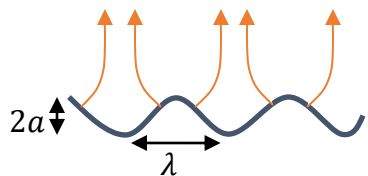
Cathode Type	Cathode	Typical Wavelength, $\lambda_{opt}$ (nm), (eV)	Quantum Efficiency (electrons per photon)	Vacuum for 1000 Hrs (Torr)	Gap Energy + Electron Affinity, $E_A + E_G$ (eV)	Thermal Emittance (microns/mm(rms))	
						Theory	Expt.
PEA: Mono-alkali	Cs <sub>2</sub> Te	211, 5.88	$\sim 0.1$	$10^{-9}$	3.5 [42]	1.2	$0.5 \pm 0.1$ [35]
		264, 4.70	-	-	"	0.9	$0.7 \pm 0.1$ [35]
		262, 4.73	-	-	"	0.9	$1.2 \pm 0.1$ [43]
	Cs <sub>3</sub> Sb	432, 2.87	0.15	?	$1.6 + 0.45$ [42]	0.7	?
	K <sub>3</sub> Sb	400, 3.10	0.07	?	$1.1 + 1.6$ [42]	0.5	?
PEA: Multi-alkali	Na <sub>3</sub> Sb	330, 3.76	0.02	?	$1.1 + 2.44$ [42]	0.4	?
	Li <sub>3</sub> Sb	295, 4.20	0.0001	?	?	?	?
	Na <sub>2</sub> KSb	330, 3.76	0.1	$10^{-10}$	$1 + 1$ [42]	1.1	?
	(Cs)Na <sub>3</sub> KSb	390, 3.18	0.2	$10^{-10}$	$1 + 0.55$ [42]	1.5	?
	K <sub>2</sub> CsSb	543, 2.28	0.1	$10^{-10}$	$1 + 1.1$ [42]	0.4	?
NEA	GaAs(Cs,F)	532, 2.33	$\sim 0.1$	?	$1.4 \pm 0.1$ [42]	0.8	$0.44 \pm 0.01$ [44]
		860, 1.44	-	?	"	0.2	$0.22 \pm 0.01$ [44]
	GaN(Cs)	260, 4.77	-	?	$1.96 + ?$ [44]	1.35	$1.35 \pm 0.1$ [45]
	GaAs(1-x)Px x $\sim 0.45$ (Cs,F)	532, 2.33	-	?	$1.96 + ?$ [44]	0.49	$0.44 \pm 0.1$ [44]
S-1	Ag-O-Cs	900, 1.38	0.01	?	0.7 [42]	0.7	?



# Simple metallic cathodes are not so simple

- Cu, most widely used, happen to be the cavity wall material
- 3-step model (excite, transport, escape) used to explain Cu
- Surface composition and morphology play significant roles

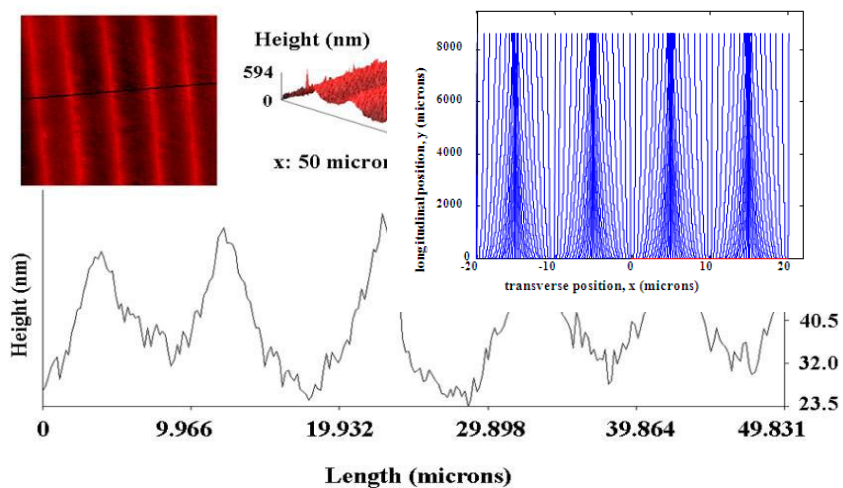
## Physical Roughness



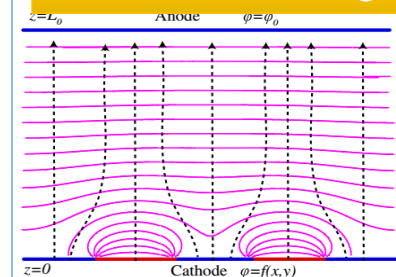
$$\text{MTE}_{\text{field}} = \frac{\pi^2 a^2 E_0 e}{2\lambda}$$

J. Feng, S. Karkare *et al*, J. Appl. Phys. 121, 044904 (2017)

Modulation amplitude = 20 nm  
Spatial wavelength = 10 microns  
Emittance = 0.15 microns /mm-rms



## Chemical Roughness

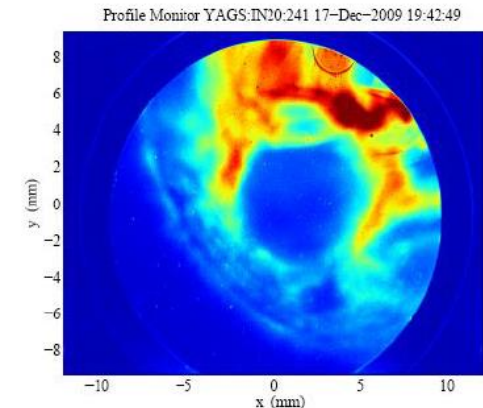


Equipotential lines Electron trajectory

S. Karkare and I. Bazarov, Phys. Rev Applied, 4, 024015 (2015)

G. Gevorkyan *et al*. PRAB, 21, 093401(2018)

$$\text{MTE}_{wf} = \frac{\pi^2 h^2 e}{4\sqrt{2} a E_0}$$



- Surface chemistry
- Morphology
- Optical absorption
- Electron scattering

Electron beam emission image of the cathode after  
>1 yr of operation

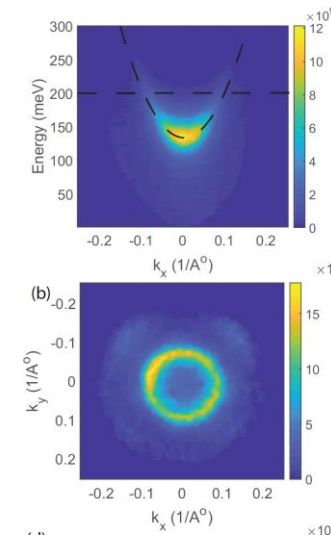
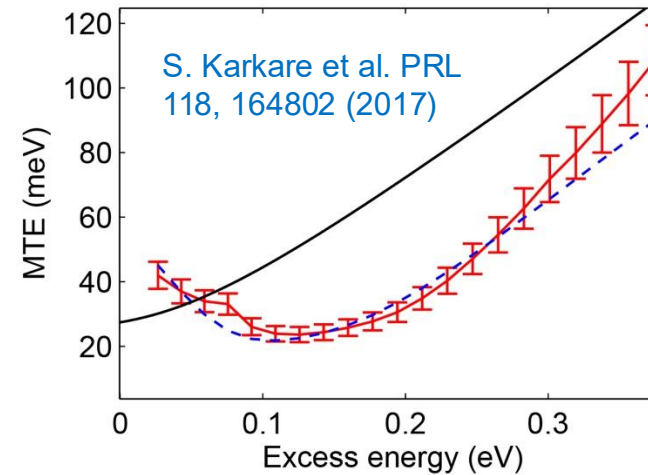
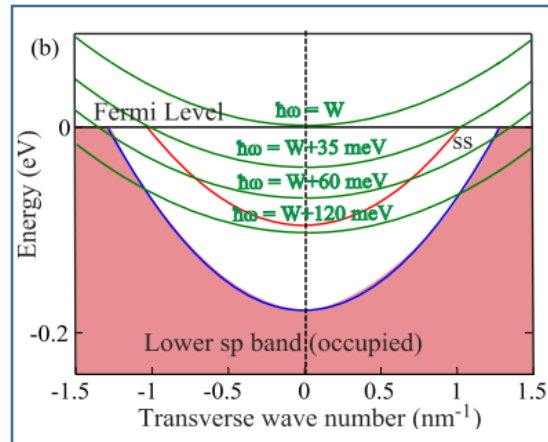




# Ordered, Clean surface

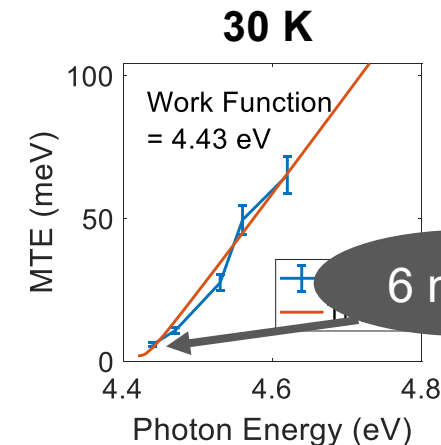
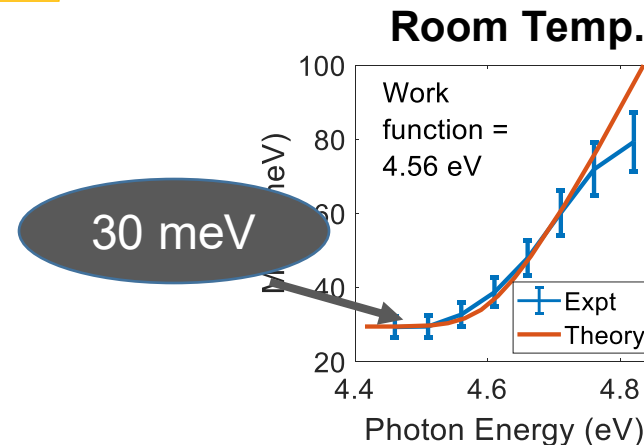
- Laser skin depth typically  $\sim 10$  nm for metallic photocathodes
- Clean, order surface has distinct band structure and can emit in one step

## Effect surface state of Ag(111)



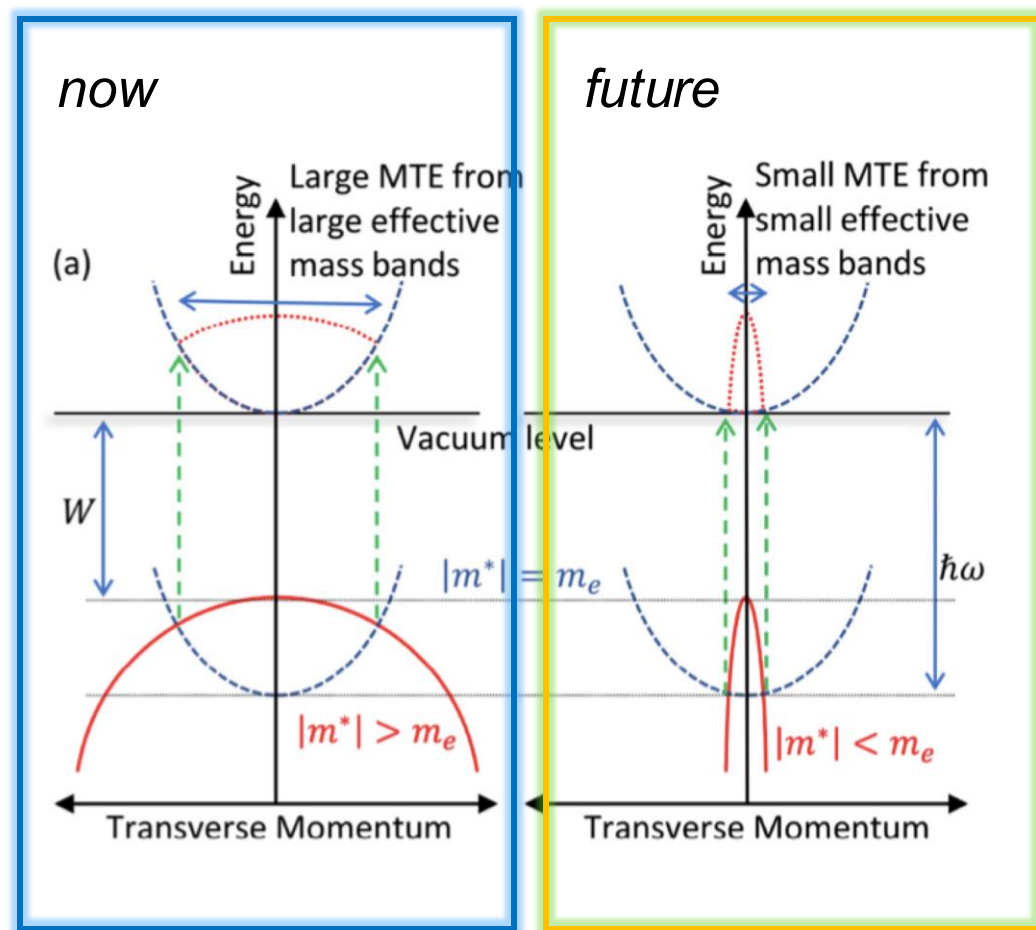
Room temp.  
25 meV

## Cooled, clean Cu(100) surface



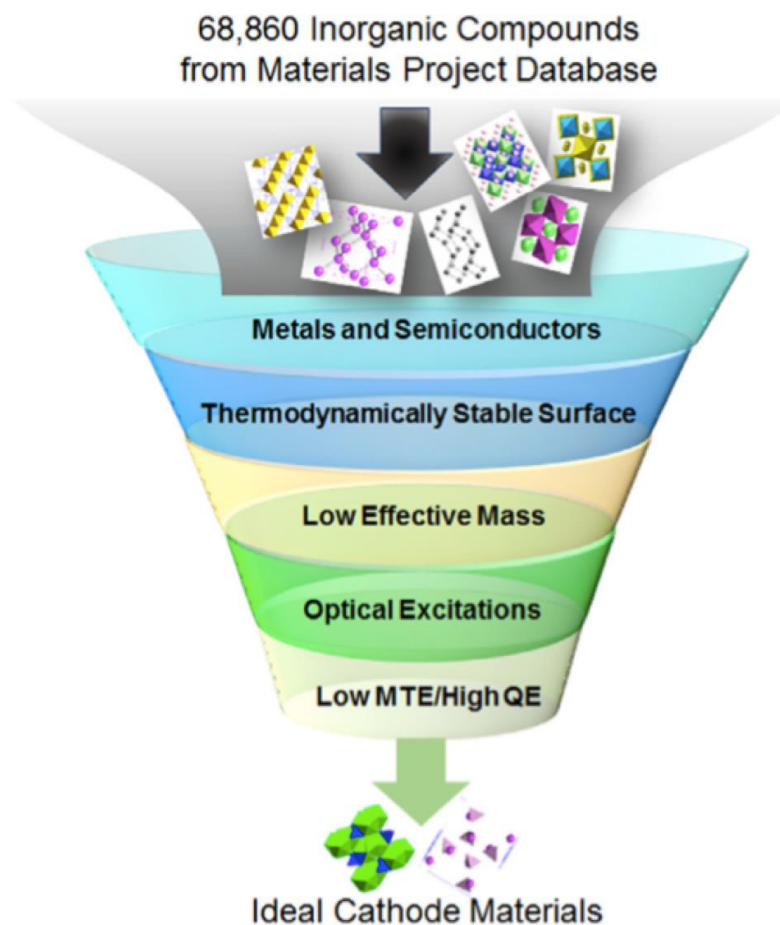
S. Karkare et al. talk at  
2018 P3 Meeting

- Engineer materials with small effective mass & crystal- $k$  conservation



Center for bright beam (CBB) website

- Computational screening of candidate materials





- Some topics in an electron gun
  - Emittance and phase space
  - Cathode and electron emission
  - Beam emittance in photo-cathode gun



# Beam dynamics in photocathode RF gun

- Motion equation of an electron in electromagnetic field

$$\frac{d\mathbf{p}}{dt} = \mathbf{F} = e(\mathbf{E} + \mathbf{v} \times \mathbf{B})$$

- Acceleration by longitudinal E-field

$$\frac{dp_z}{dt} = F_z = eE_z$$

- Transverse bending/focusing/defocusing

$$\frac{dp_x}{dt} = F_x = e(E_x - v_z B_y)$$

$$\frac{dp_y}{dt} = F_y = e(E_y + v_z B_x)$$

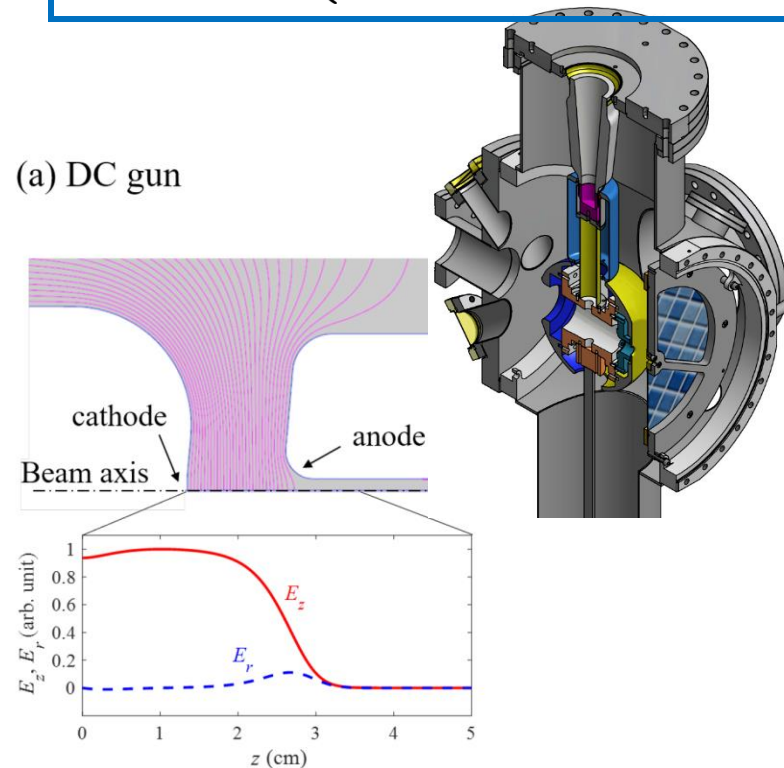
$$\frac{dp_r}{dt} = F_r = e(E_r - v_z B_\theta)$$

$(r, \theta, z)$  coordinate

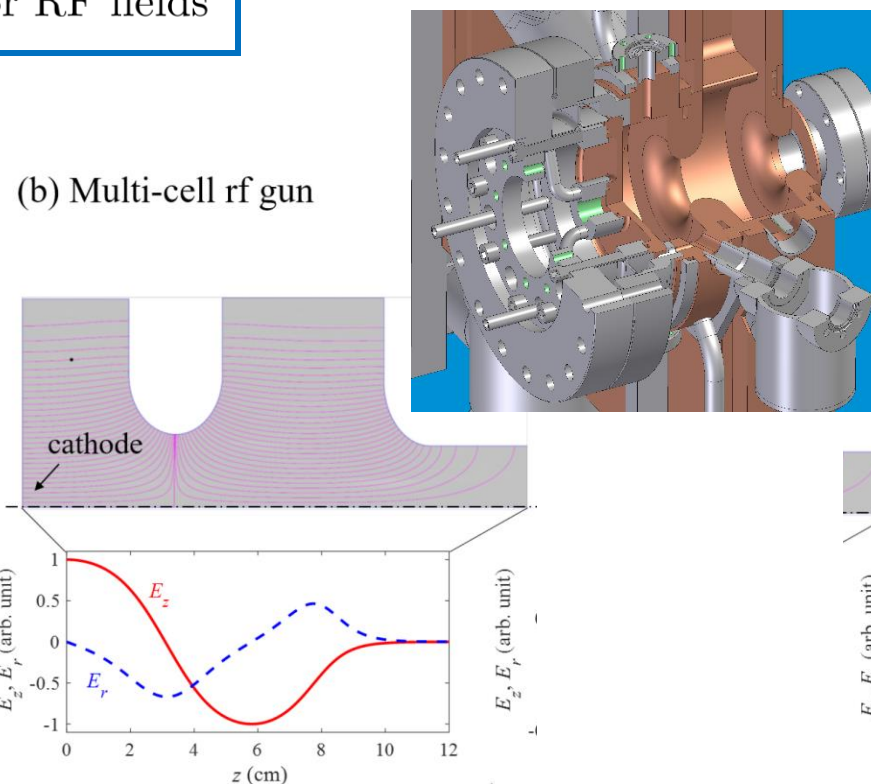


- Guns designed with quite different field distribution and strength
- DC gun, RF gun

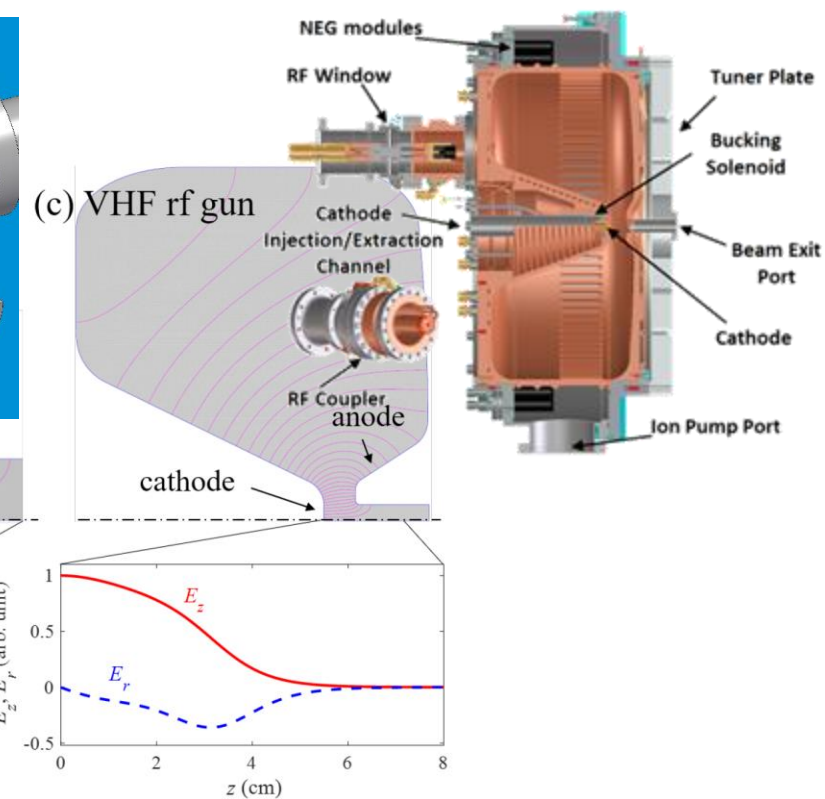
$$E_z(z, r, t) = \begin{cases} E_0 e_z(z, r) & \text{for DC fields} \\ E_0 e_z(z, r) \sin(\omega t + \phi) & \text{for RF fields} \end{cases}$$



5-10MV/m



~100MV/m



20-30MV/m



- DC gun

$$E(z, r, t) = E_0 e(z)$$

$$\frac{d\gamma}{dz} = \frac{eE_0 e(z)}{2mc^2} \quad \gamma = \int_0^z \frac{d\gamma}{dz} dz = \frac{eE_0 \int_0^z e(z) dz}{2mc^2}$$

- RF gun (standing wave structure)

$$E(z, r, t) = E_0 e(z) \sin(\omega t + \phi_0)$$

define electron phase with respect to rf field as

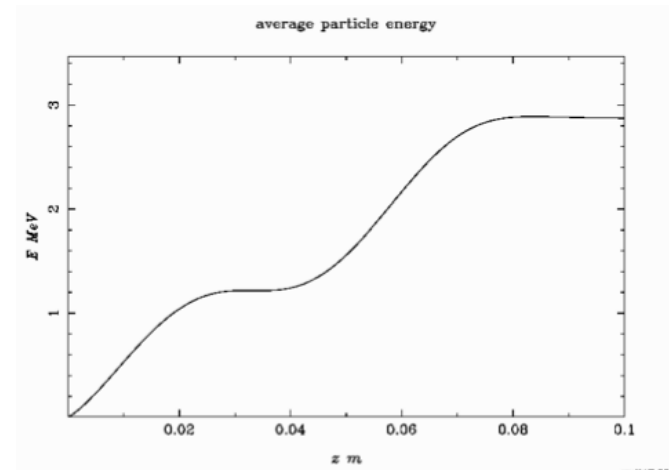
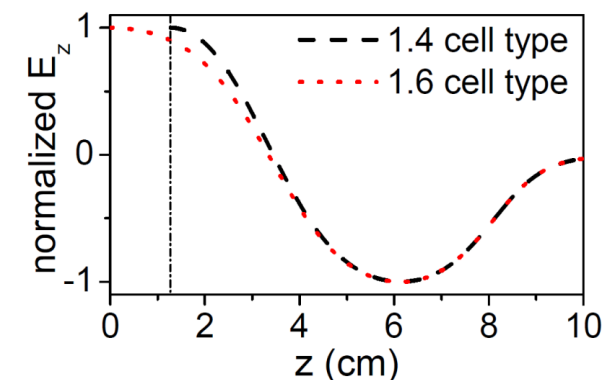
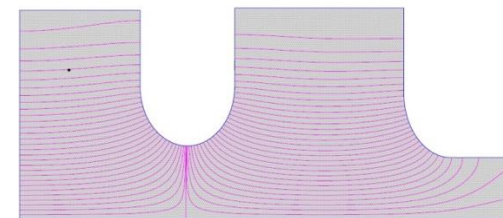
$$\phi = \omega t - kz + \phi_0 \quad \text{or} \quad \phi = k \int_0^z \left( \frac{\gamma}{\sqrt{\gamma^2 - 1}} \right) dz + \phi_0$$

$$\frac{d\gamma}{dz} = \frac{eE_0 e(z) \sin(\omega t + \phi_0)}{2mc^2} \quad \text{can be calculated with Runge-Kutta method}$$

For 1.5cell pi-mode RF gun,  $E(z, r, t) \approx E_0 \cos kz \sin(\omega t + \phi_0)$

$$\frac{d\gamma}{dz} = \frac{eE_0 [\sin(\phi) + \sin(\phi + 2kz)]}{2mc^2}$$

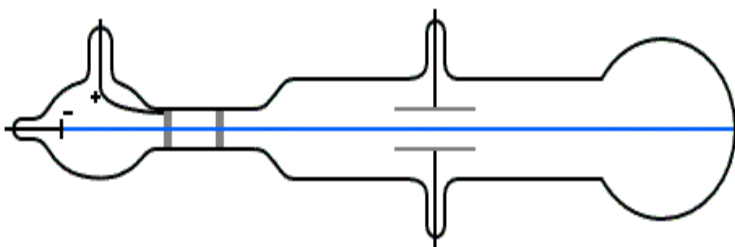
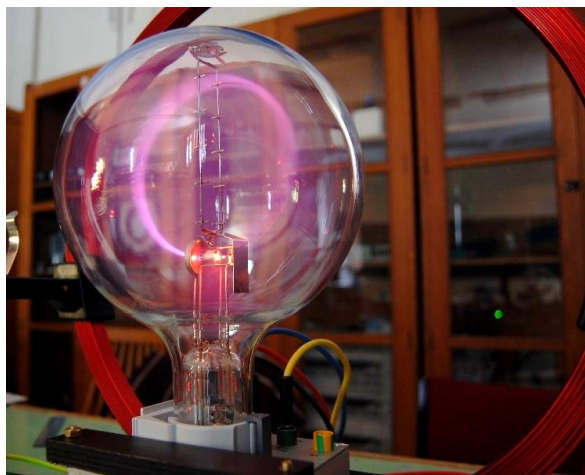
## 1.6 cell type



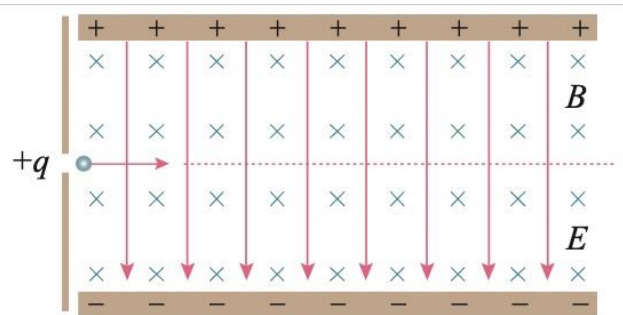




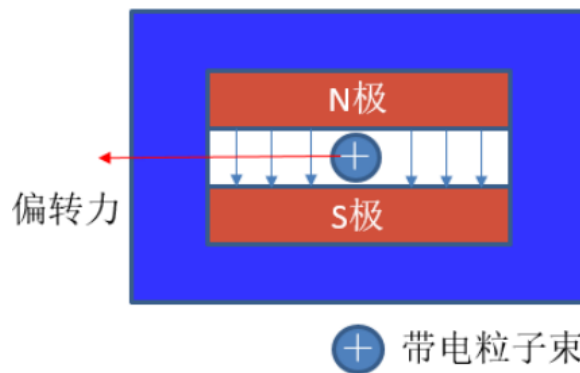
$$\frac{dp_x}{dt} = F_x = e(E_x - v_z B_y)$$



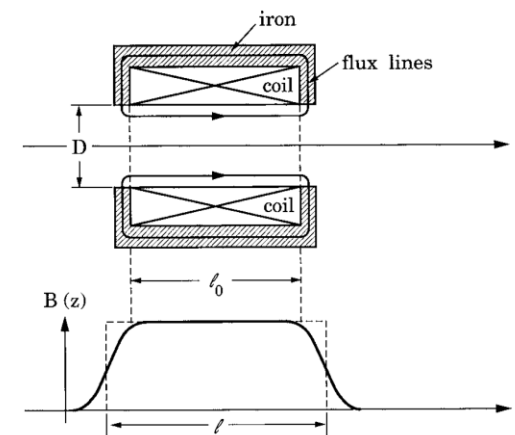
## 带电粒子速度选择器



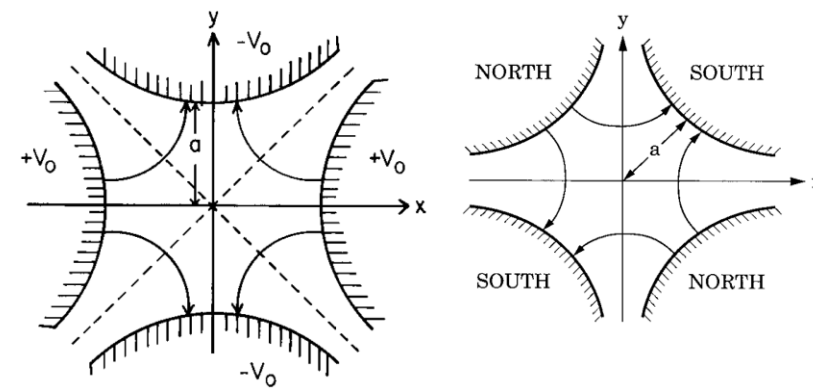
$$v = E/B$$



$$p = erB$$



$$\frac{1}{f} = -\frac{\Delta r'}{r} = \left( \frac{e}{2mc\beta\gamma} \right)^2 \int_{z_1}^{z_2} B^2 dz$$



$$\kappa = \frac{eV_0/a}{\gamma\beta^2 m_0 c^2}$$

$$\kappa = \frac{eB_0/a}{\gamma\beta m_0 c}$$



# Emittance growth due to rf field

- With longitudinal E-field  $E_z$ , transverse fields can be found from Maxwell equations(paraxial approximation):

$$E_r = -\frac{r}{2} \frac{\partial E_z}{\partial z} \quad eB_\theta = \frac{r}{2} \frac{\partial E_z}{\partial t}$$

$$F_r = e(E_r - \beta c B_\theta) - \frac{r}{2} \frac{\partial E_z}{\partial z} \quad E(z, r, t) = E_0 e(z) \sin(\omega t + \phi_0) \approx E_0 \cos(kz) \sin(\omega t + \phi_0)$$

$$F_r = er \left\{ -\frac{1}{2c} \frac{d}{dt} [E(z) \sin kz \cos(\omega t + \phi_0)] - \frac{1}{2} \left[ \frac{dE(z)}{dz} \right] \cos kz \sin(\omega t + \phi_0) + \frac{\beta}{2} \left[ \frac{dE(z)}{dz} \right] \sin kz \cos(\omega t + \phi_0) \right\}$$

Assume transverse deflection is small, r can be regards as constant and integrate the equation of radial motion give the radial impulse

$$p_r = \frac{1}{mc} \int_0^f F_r dt$$

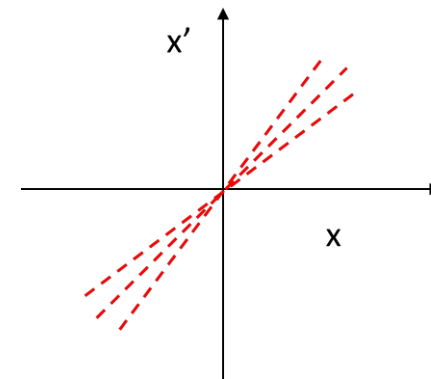
0 for axial symmetric field

$$p_r = p_{r0} + \alpha kr [\beta \cos z_f \sin(\omega t + \phi_0) - \sin kz_f \cos(\omega t + \phi_0)] \approx \alpha kr \sin \phi$$

Phase dependence

Emittance increase due to transverse rf field:

$$\varepsilon_x^{rf} = \sqrt{\langle x^2 \rangle \langle p_x^2 \rangle - \langle x p_x \rangle^2} \approx \alpha kr \langle x^2 \rangle \sqrt{\langle \sin^2 \phi \rangle - \langle \sin \phi \rangle^2} \approx \frac{eE_0}{2mc^2} \frac{\langle x^2 \rangle \sigma_\phi^2}{\sqrt{2}}$$



# Emittance growth due to multipole field in gun

- Previous page gives the emittance growth due to monopole field in the gun
- Non-axisymmetric structure excites multipole field components, such as the dipole, quadrupole, and octopole, which kick the beam time dependently, leading to the emittance growth

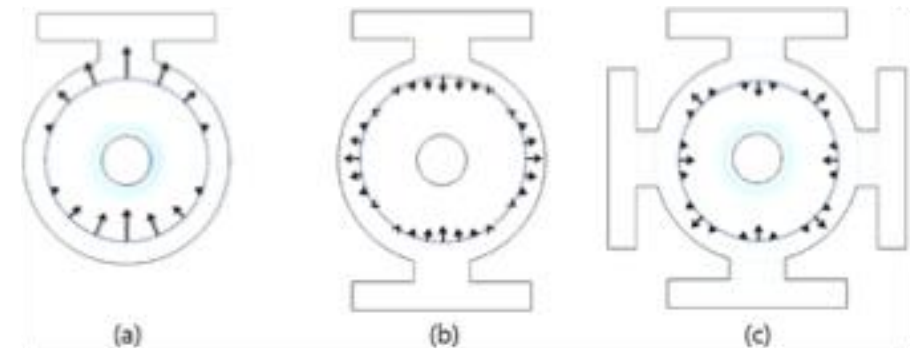
$$E_z^{110} \approx E_1 \sin(\omega t + \phi_0) \cos(kz) J_1(k_c r) \cos\left(\theta - \frac{\pi}{2}\right) = \alpha_{110} E_0 \sin(\omega t + \phi_0) \cos(kz) y$$

$$p_y^{110} \approx -\alpha_{110} \alpha L \sin \phi_0 \hat{y}$$

$$\varepsilon_{n,y}^{110} \approx \alpha_{110} \alpha L \cos \phi_0 \sigma_y \sigma_\phi$$

$$E_z^{210} \approx \alpha_{210} E_0 \sin(\omega t + \phi_0) \cos(kz) (x^2 + y^2)$$

$$\varepsilon_{n,y}^{210} \approx 2\alpha_{210} \alpha L \cos \phi_0 \sigma_y^2 \sigma_\phi$$



Schematic drawing of each multipole mode in the rf gun. (a) Dipole mode. (b) Quadrupole mode. (c) Octopole mode.

$\alpha_{110}, \alpha_{210} : \sim 10^{-4}$  to  $10^{-6}$  for fine designed RF structure, emittance growth :  $\sim 0.01$ - $0.1$  mm mrad

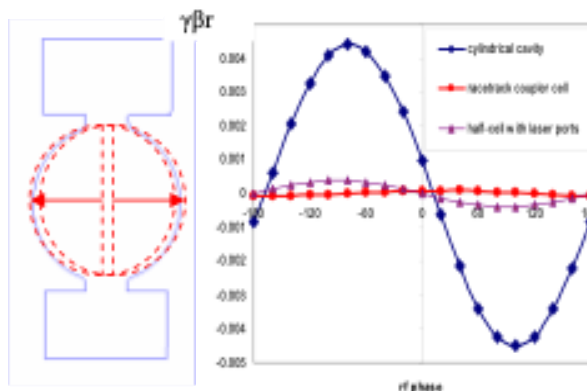
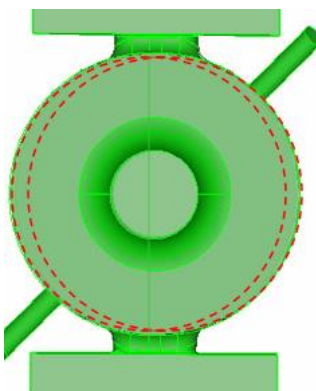


# Emittance growth due to multipole field in gun

Structure design to eliminate the multipole

SLAC LCLS gun design

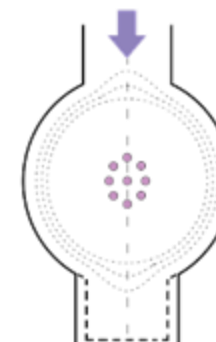
Dual feed + racetrack



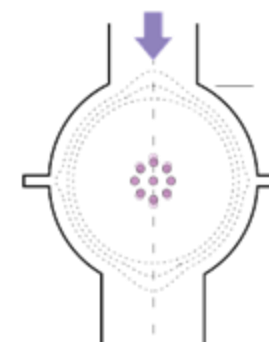
Tsinghua gun design



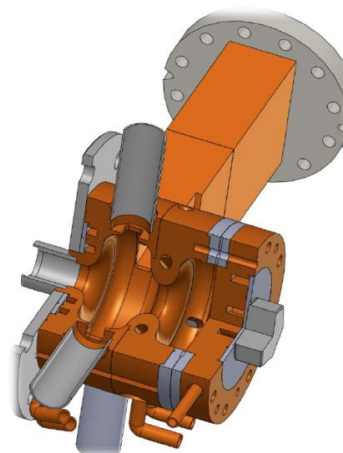
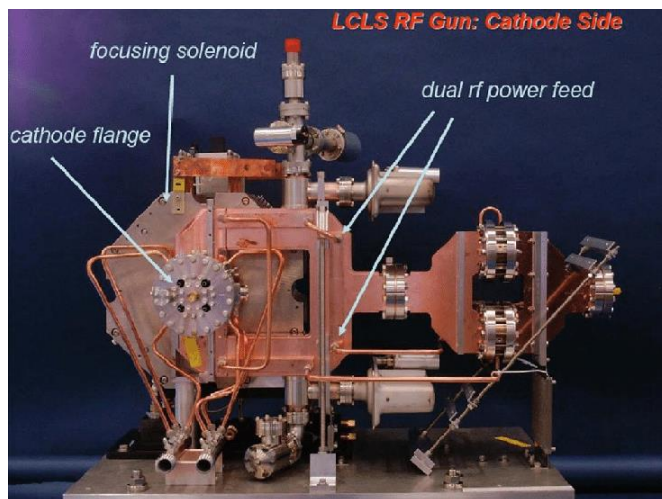
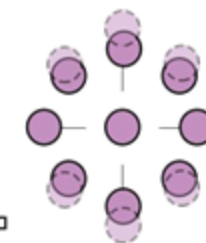
同型  
对称孔



优化  
对称孔



四孔  
对消



Houjun Qian et. al, NIMA 597, 121 (2008)

Xin Guan et. al, NIMA 574, 17 (2007)



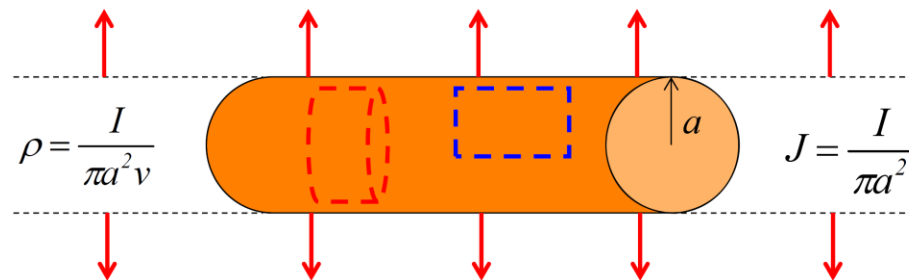
- For infinite length, uniform beam, the E-M field generated by beam:

$$\int \epsilon_0 E \cdot dS = \int \rho dV \quad \int B \cdot dl = \int \mu_0 J \cdot dS$$

$$2\pi r l \cdot \epsilon_0 E_r = \rho \cdot \pi r^2 l \quad B_\theta \cdot 2\pi r = \mu_0 J \cdot \pi r^2$$

$$E_r = \frac{\rho r}{2\epsilon_0} = \frac{I r}{2\pi\epsilon_0 a^2 v} \text{ for } r \leq a$$

$$B_\theta = \frac{\mu_0 J r}{2} = \frac{\mu_0 I r}{2\pi a^2} \text{ for } r \leq a$$



- The force to the electron

$$F_r = e(E_r - \beta c B_\theta) = e(1 - \beta^2)E_r = \frac{eE_r}{\gamma^2}$$

- Equation of motion:

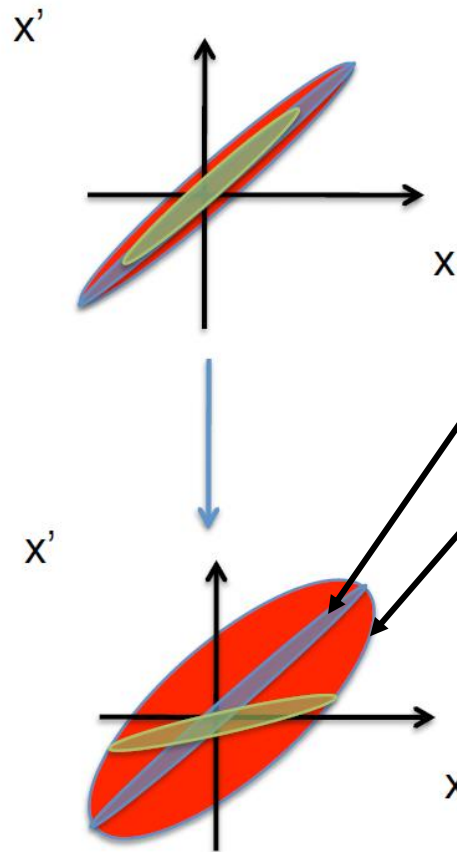
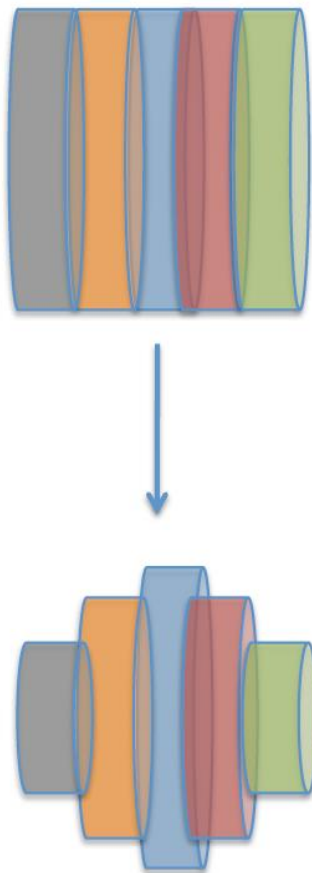
$$\frac{d^2 r}{dz^2} = \frac{eI}{2\pi m \gamma^3 \epsilon_0 a^2 v^3} r = \frac{K}{a^2} r, \text{ 其中 } K = \frac{2I}{I_A (\beta \gamma)^3}, I_A = \frac{4\pi \epsilon_0 m c^3}{e}$$





# Emittance growth due to space charge (SC) forces

- Beam dynamics are almost **decoupled** in longitudinal and transverse directions
- Thus we usually treat the entire beam as many slices
- SC acts as **defocusing** lens, and the strength  $\propto$  charge density of each slice
- There is slight different for each slice with finite length bunch



Slice emittance

Projected emittance

Important literatures on emittance compensation:

K.-J. Kim, NIMA 275, 201 (1988)

B. Carlsten, NIMA 285, 313 (1989)

L. Serafini and J. Rosenzweig, PRE 55, 7565 (1997)

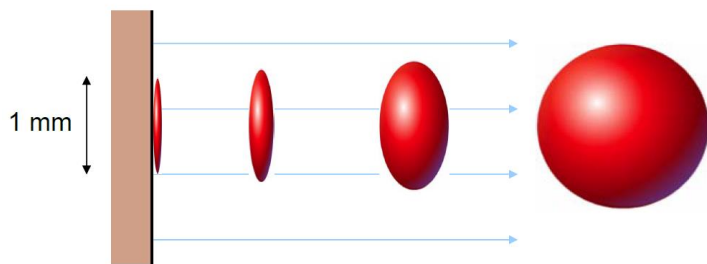
S.C. Anderson, PhD Thesis (2002)

M. Ferrario et al., PRL 104, 054801 (2010)





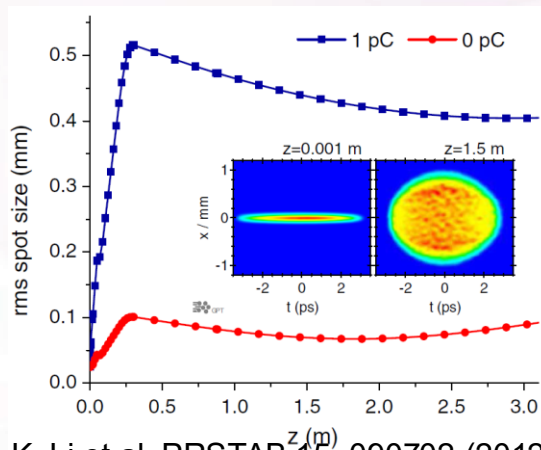
**Pancake:** a transversely spherical, ultrashort electron beam



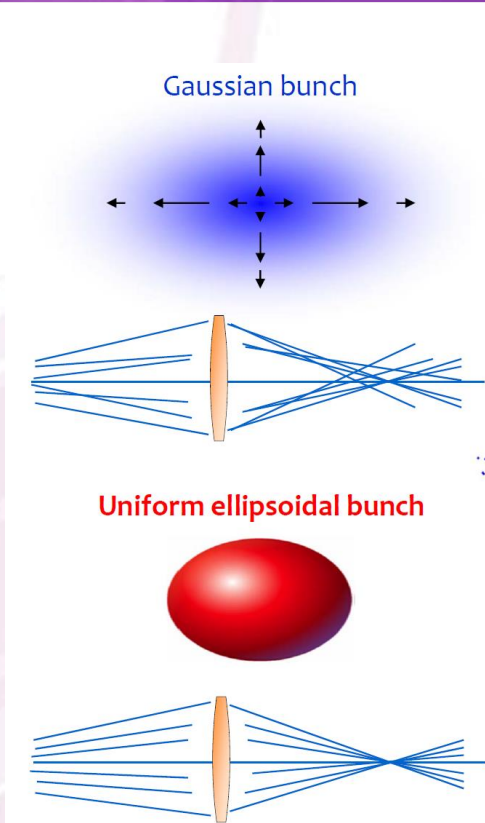
Luiten et al., PRL 93, 094802 (2004)

**Cigar:** a longitudinally parabolic, relatively long electron beam

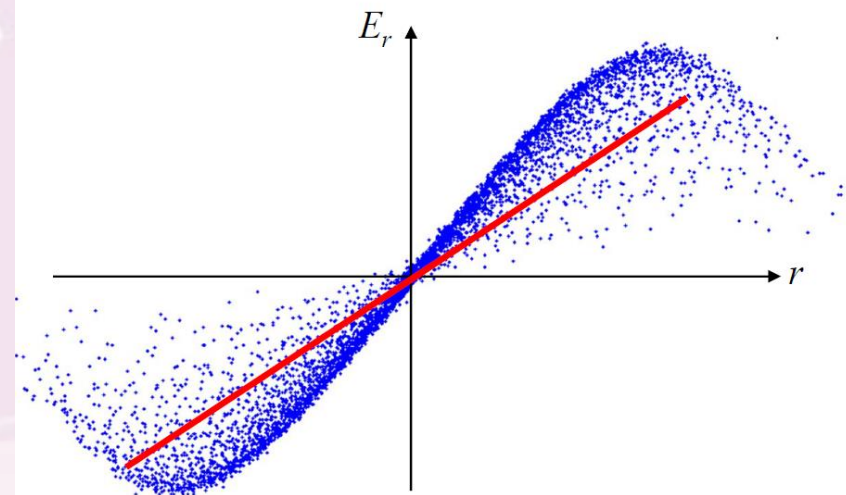
- Transverse expansion
- Much lower emittance (10s of nm)



R. K. Li et al, PRSTAB 15, 090702 (2012)



**Nonlinear** space-charge forces;  
**Irreversible** Coulomb expansion



**Linear** space-charge forces;  
**Reversible** Coulomb expansion

$$\left(\frac{x}{A}\right)^2 + \left(\frac{y}{B}\right)^2 + \left(\frac{z}{C}\right)^2 = 1$$

$$\vec{E} = (E_x, E_y, E_z) = \frac{\rho_0}{\epsilon_0} (M_x x, M_y y, M_z z)$$

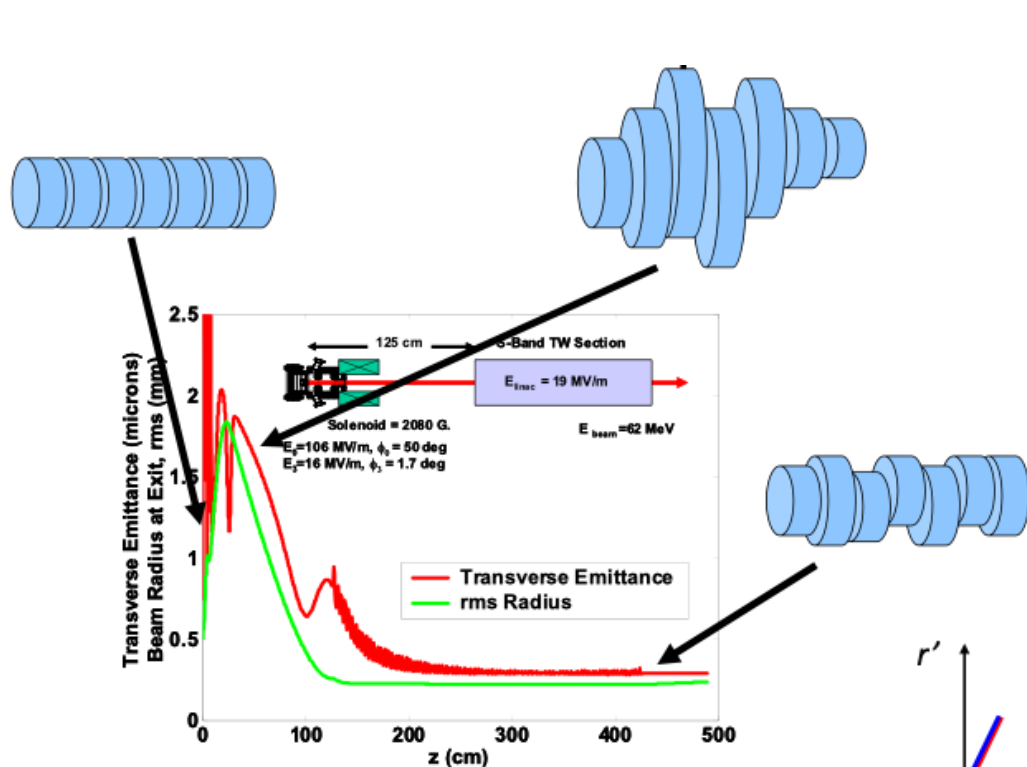
Kapchinskii and Vladimirskii, 1959  
Luiten et al., PRL 93, 094802 (2004)



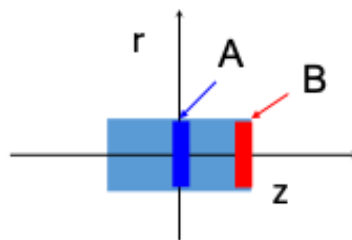


# Emittance oscillation and compensation in a photo-injector

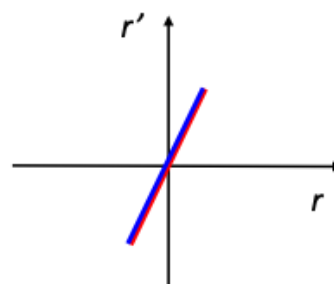
- slice phase space is rotated and oscillation with rf field, space charge force, solenoid focusing field
- Emittance due to the linear space charge force, rf field, solenoid can be compensated, but it's not all
- minimum projected emittance achieves when phase space of most of slices are aligned



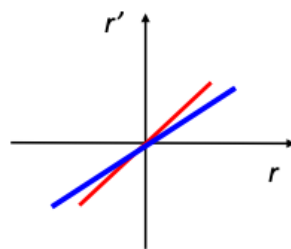
Evolution of normalized RMS emittance and RMS beam size



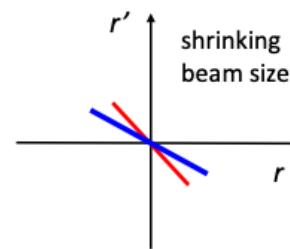
an electron bunch from the photocathode rf gun, particles near A experience different space charge force from particles near B



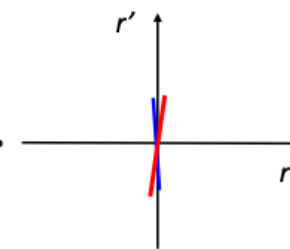
beam at gun exit



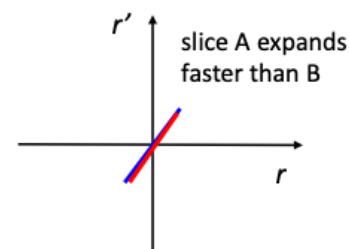
after a drift section



after focusing solenoid



close to focal point of slice A



after focal point of slice A

Important literatures on emittance compensation:

K.-J. Kim, NIMA 275, 201 (1988)

B. Carlsten, NIMA 285, 313 (1989)

L. Serafini and J. Rosenzweig, PRE 55, 7565 (1997)

S.C. Anderson, PhD Thesis (2002)

M. Ferrario et al., PRL 104, 054801 (2010)

- Total emittance of a beam from photo-injector

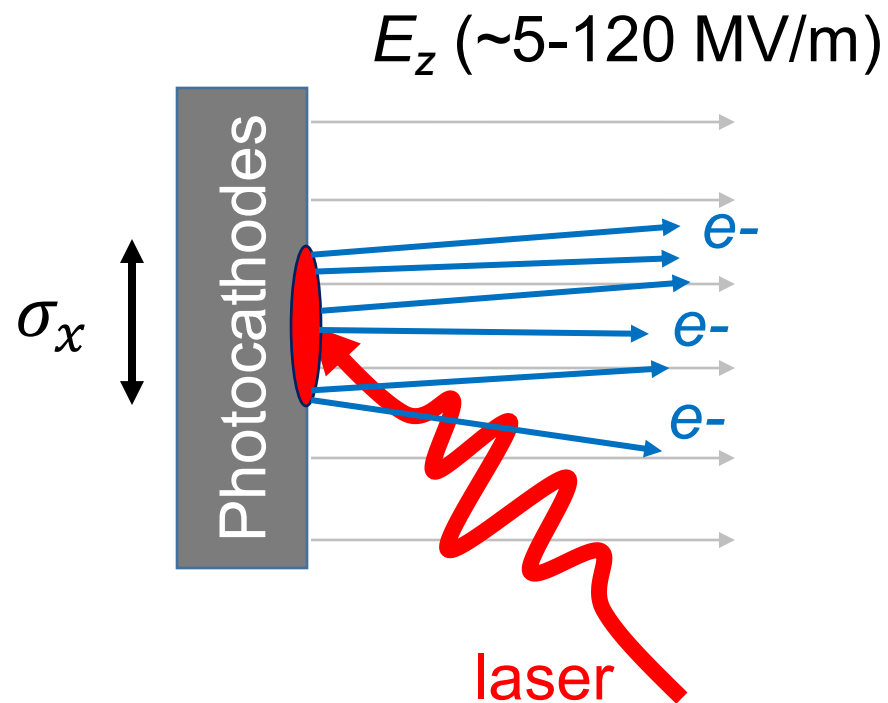
$$\varepsilon_{total} = \sqrt{\varepsilon_{thermal}^2 + \varepsilon_{rf}^2 + \varepsilon_{sc}^2 + \varepsilon_{optics}^2 + \dots}$$

$\varepsilon_{thermal}$  : initial emittance from cathode, depended on the emission process, minimum emittance which can be achieved

$\varepsilon_{rf}$ : rf field is time varying and kick the beam time dependently, leading to the emittance growth

$\varepsilon_{sc}$ : linear space charge forces effects can be compensated by solenoid; non-linear space charge forces leading to emittance growth; pulse shaping, high gun gradient are very helpful.

$\varepsilon_{optics}$ : Aberrations of magnetic lenses



4D beam brightness

$$\mathcal{B}_{4D} \propto f_e \frac{N}{(\sigma_x \cdot \sqrt{\text{MTE}})^2}$$

Mean Transverse Energy  $\text{MTE} = \frac{1}{2} m v^2$

Preservation of the brightness  $f_e$

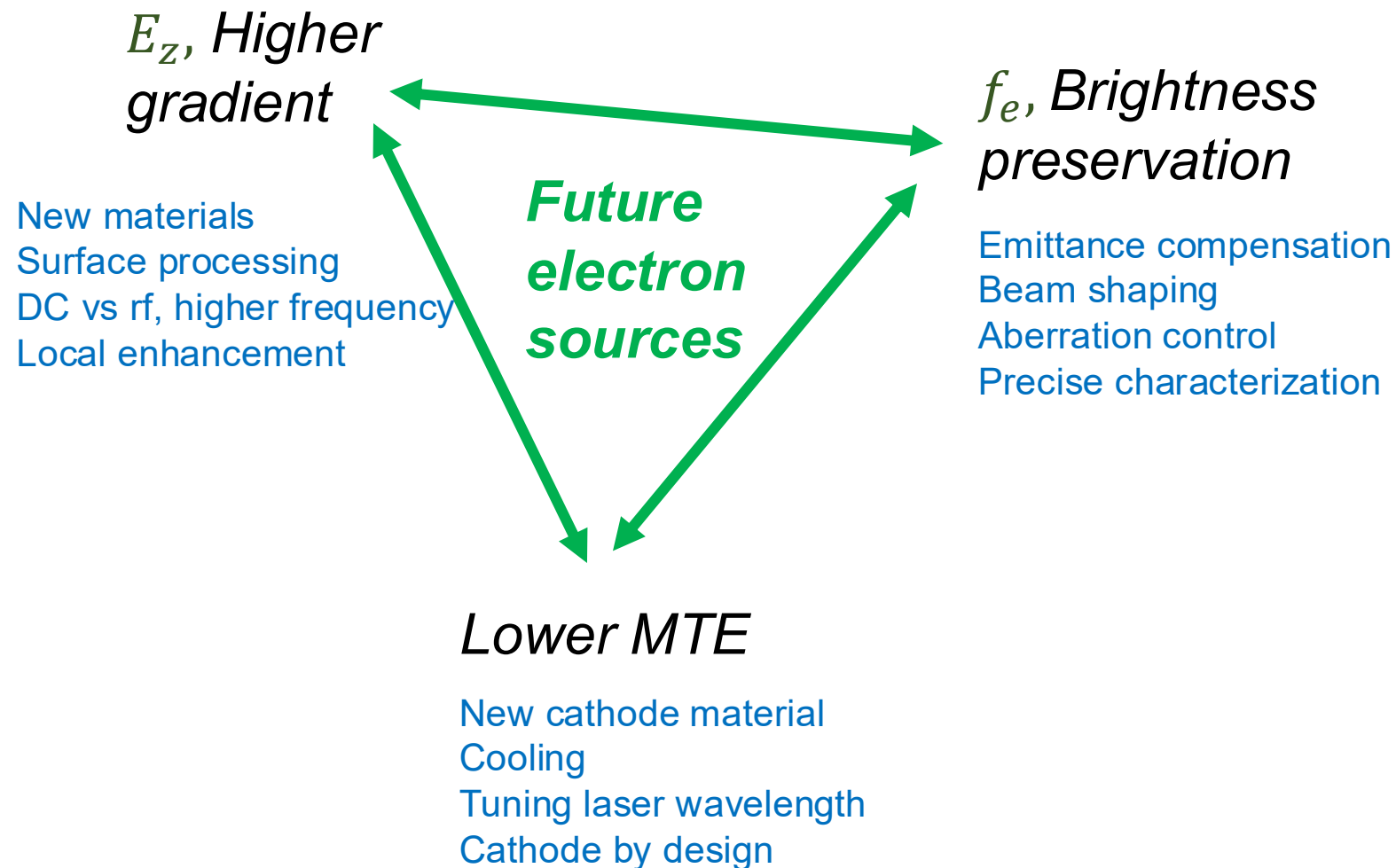
$\mathcal{B}_{4D} \propto f_e \frac{E_z}{\text{MTE}}$  for pancake ( $A \gg 1$ ) beam, where aspect ratio

PRL 102, 104801

$\mathcal{B}_{4D} \propto f_e \frac{E_z^{3/2}}{\text{MTE}} \frac{\sigma_t}{\sigma_x^{1/2}}$  for cigar shape ( $A < 1$ ) beam

$$A = \frac{\sigma_x m_e}{\sigma_t^2 E_z e}$$

PRAB 17, 024201<sub>56</sub>



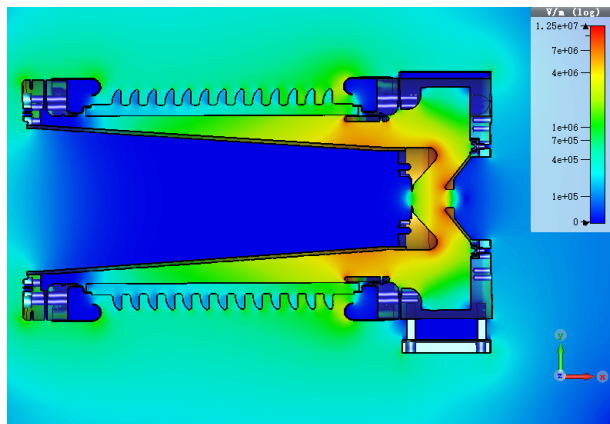
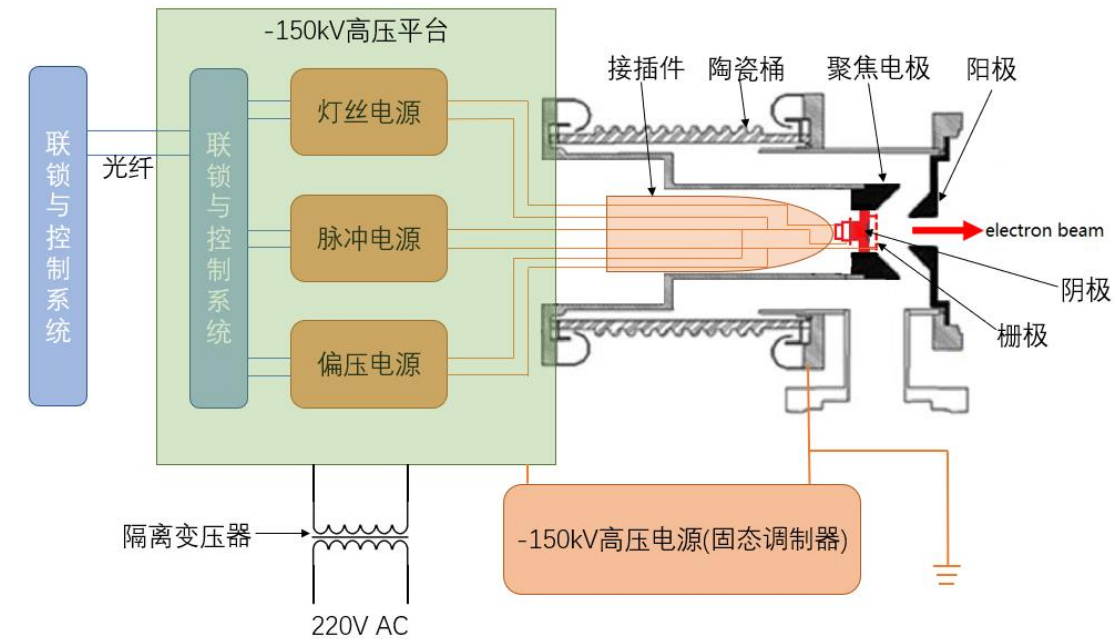


# Typical guns for accelerators



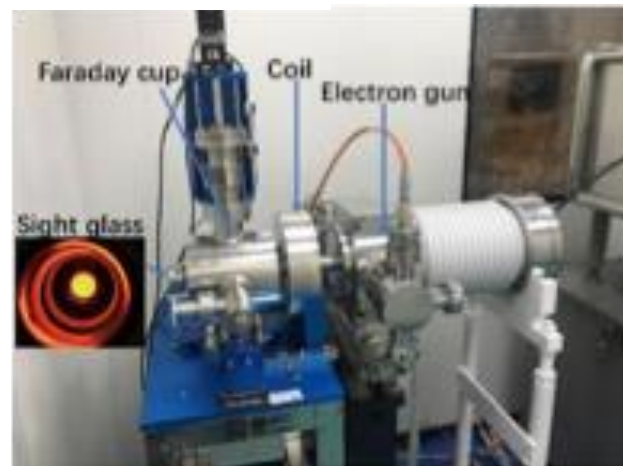


# High voltage gridded thermionic cathode electron gun



Maximum gradient at surface:~12.5MV/m

参数名称	数值	单位
宏脉冲电荷量	0.5~10	nC
束流脉冲半高全宽	$\leq 1.0$	ns
束流脉冲底宽	$\leq 1.6$	ns
非归一化4*RMS发射度	$\leq 30$	$\mu\text{m}\cdot\text{rad}$
阴极高压	$\geq 150$	kV
高压稳定度	$\leq 0.5$	%
重复频率	50	Hz
工作模式	单脉冲	-



(a)



## The 140 kV Electron Gun System for Taiwan Light Source







## 30 MeV Low Emittance Thermionic Gun Injector



500 kV, 60 Hz pulser



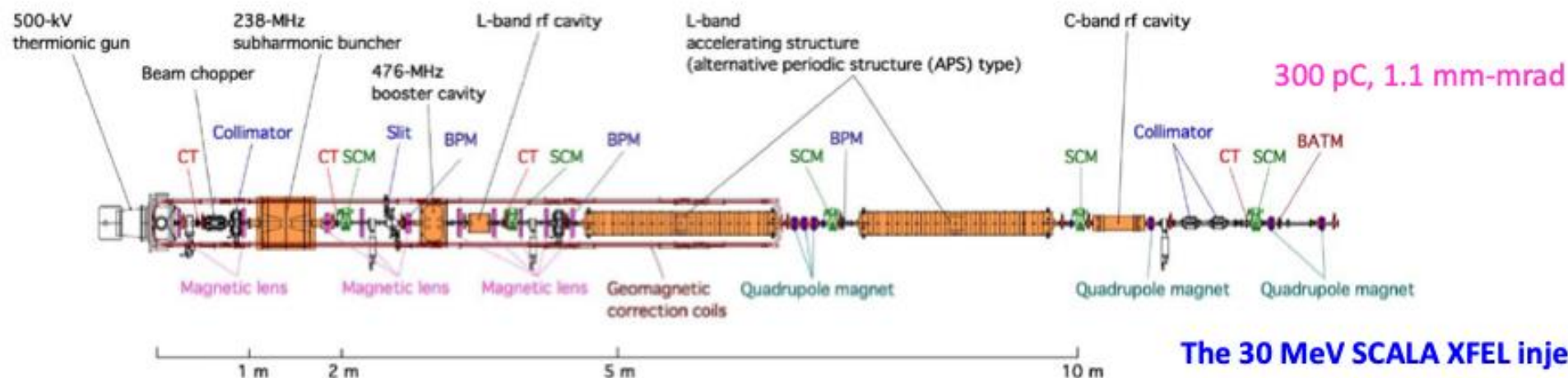
Thermionic gun with  $\phi$  3mm CeB<sub>6</sub> cathode



476 MHz booster cavity  
+ L-band correction  
cavity



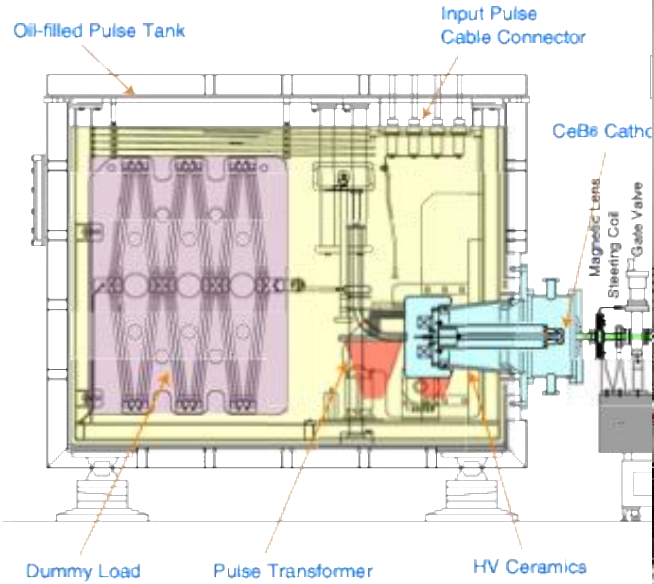
L-band linac



The 30 MeV SCALA XFEL injector

# Thermionic gun for low emittance beam(SACLA injector)

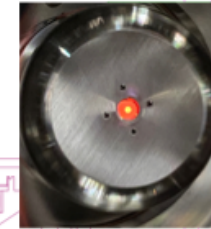
500 kV Electron Gun



## Toward ultimate-brightness thermionic electron gun

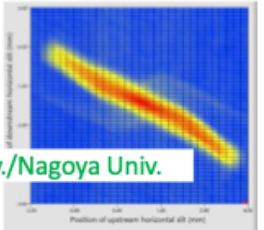
3. Low heat load and short pulse

IR-laser heating  
with AIST



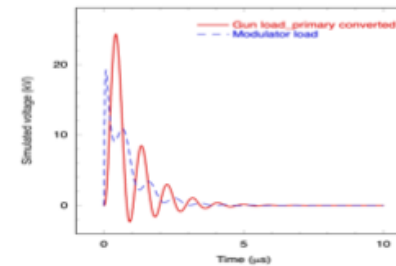
1. Small emitter

Single-crystal  $\text{CeIr}_2$   
with AIST/Kobe Univ./Nagoya Univ.



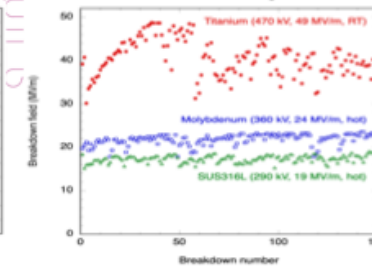
4. Short pulse

New HV circuit



2. High gradient

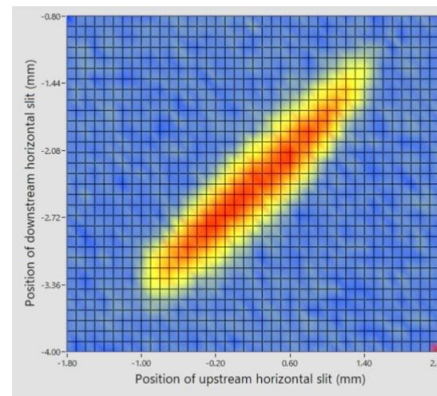
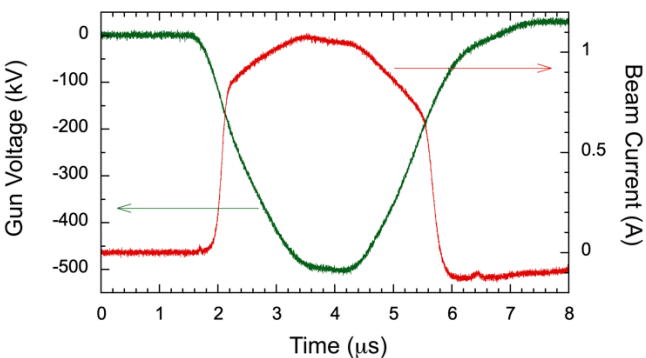
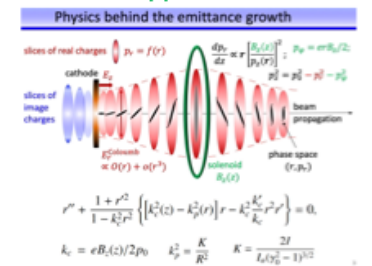
Super-clean titanium



5. Minimum aberration

Solenoid dynamics  
Hybrid magnetic lens

with Uppsala Univ.

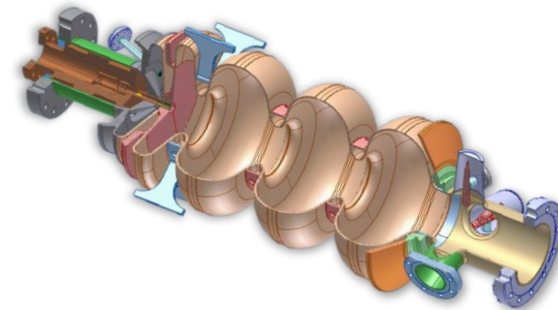
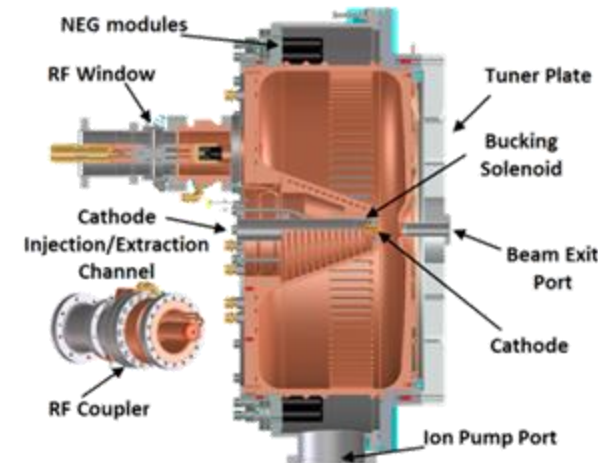
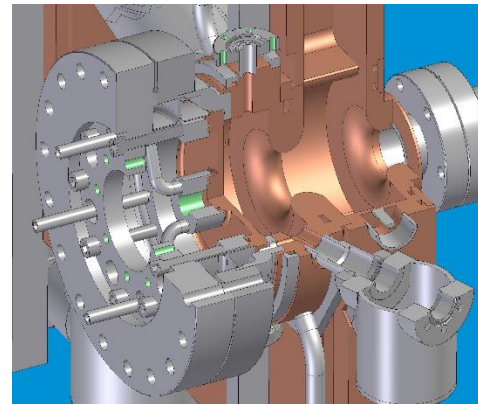
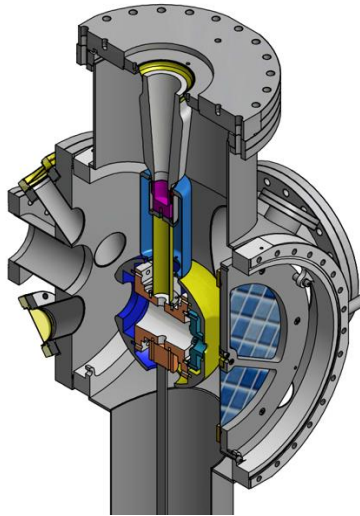


Only 1-ns cut by chopper Normalized emittance  $0.4 \mu\text{m}$





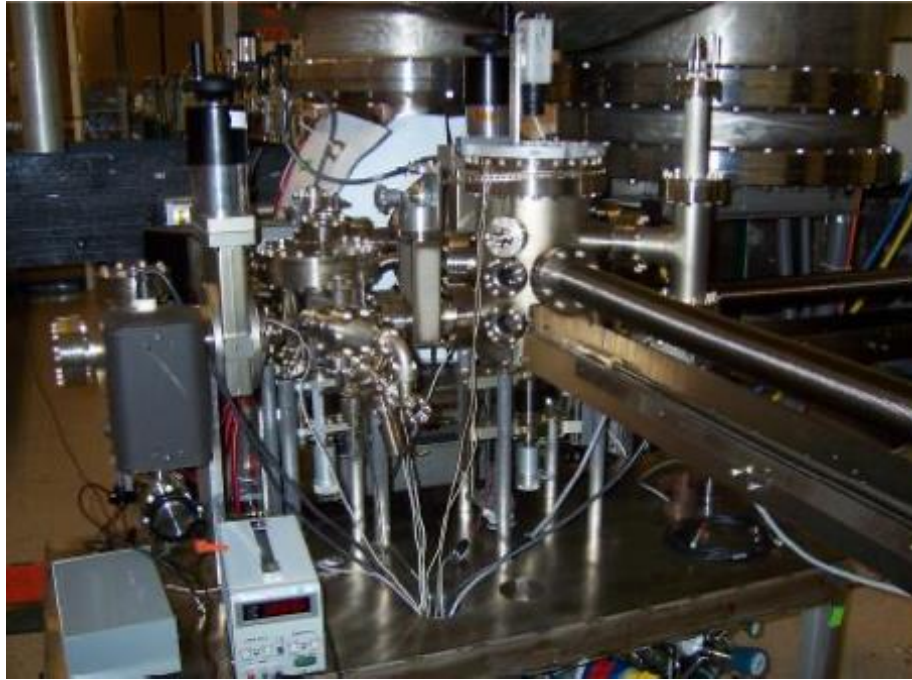
# high brightness photocathode guns



	DC	Pulsed NC RF	CW NC RF	SRF
Cathode environment	Good vacuum, cold	Worse vacuum, hot	Worse vacuum, hot	Good vacuum, cold
Gradient	<10 MV/m	~100-120MV/m	20(35) MV/m	~20(40) MV/m
Energy	<0.5 MeV	5MeV	0.75(1.5-2) MeV	>2 MeV
Main challenge	Limited gradient and energy	Limited repetition	Heat load, operation reliability	cavity-cathode joint, cavity contamination



# Cornell photocathode DC gun



- High QE cathode to minimize laser heating
- GaAs cathode, require ultra high vacuum at 10-12 mbar
- Smooth electrode surfaces to minimize field emission
- Need reliable HVDC power supply and insulator design
- Low beam energy, need more complicated injector design.
- Capability to provide sub- $\mu\text{m}$ , few hundred pC beam has been demonstrated.
- Stable operation at  $\sim 400$  kV

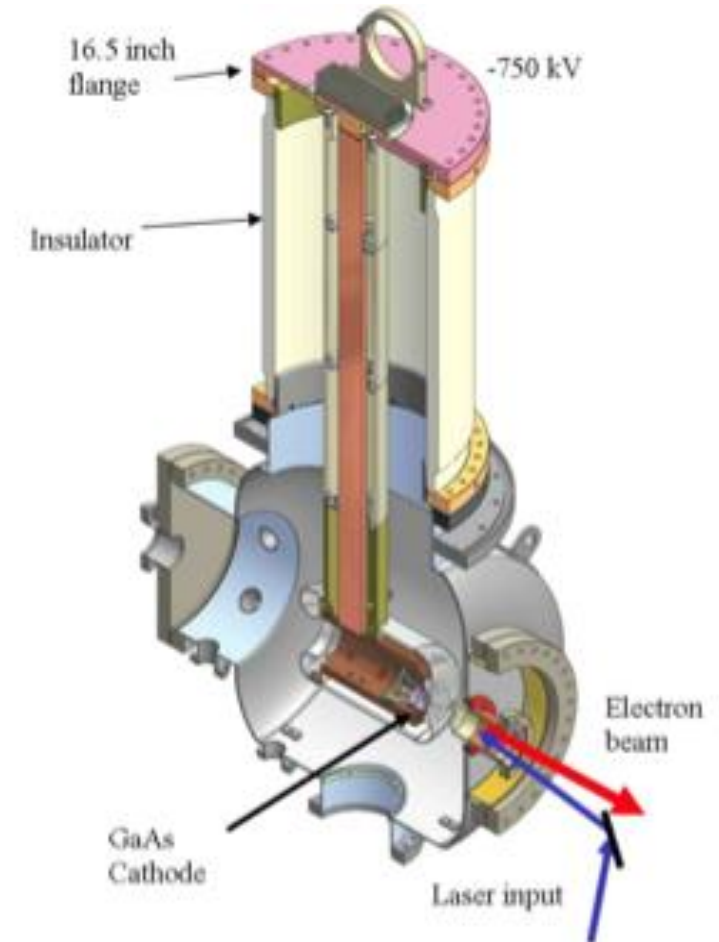
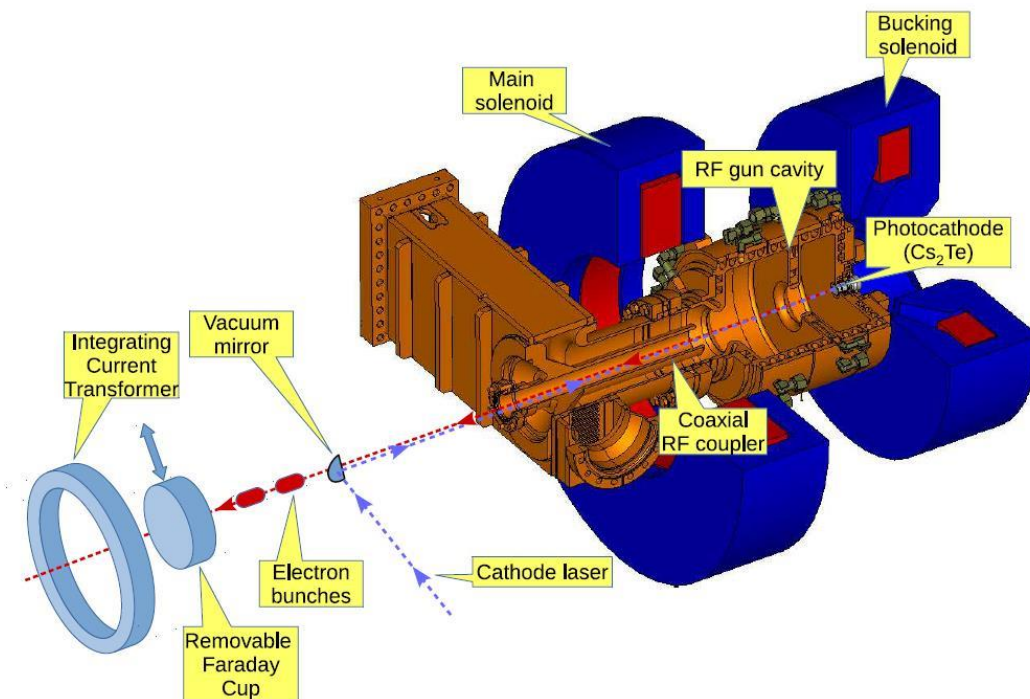


FIGURE 2. The Cornell Photoemission Gun.

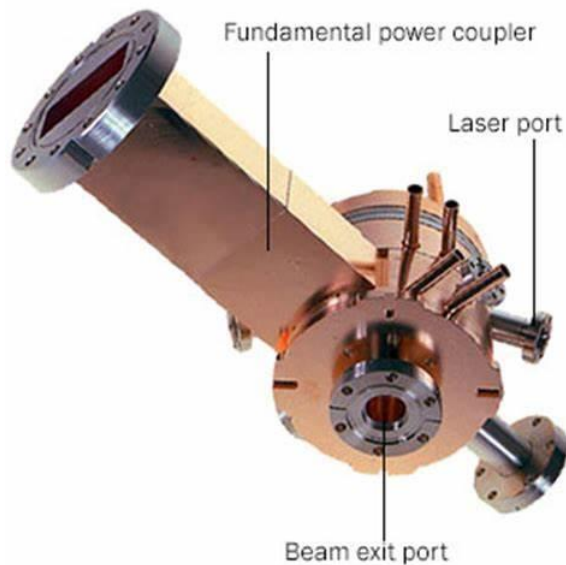


- operating frequency @ 1300 MHz
- Cs<sub>2</sub>Te cathode delivers 0.001 – 4 nC bunch charge
- Beam mean energy 6.5 MeV
- Number of electron pulses in bunch train < 800
- Macro pulse repetition rate 10Hz
- Bunch rep.-rate 10kHz
- Average beam current 32  $\mu$ A max.
- Optimized emittance < 0.9  $\mu$ m

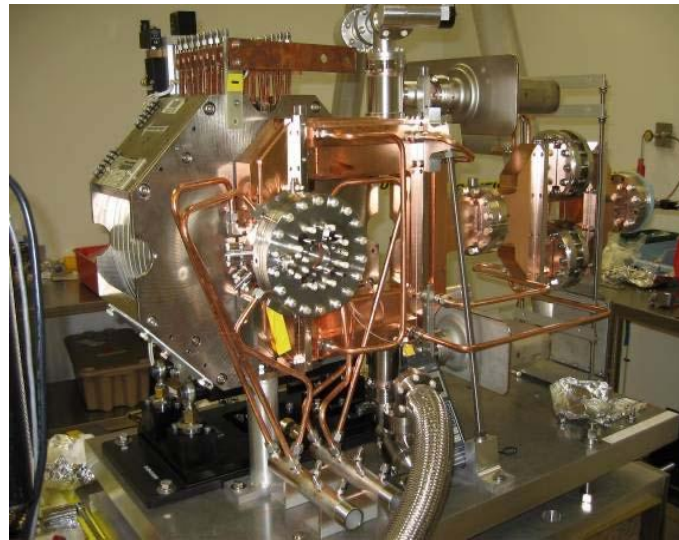


# 1.6 Cell S-band high gradient photocathode gun

BNL-type gun



SLAC LCLS gun

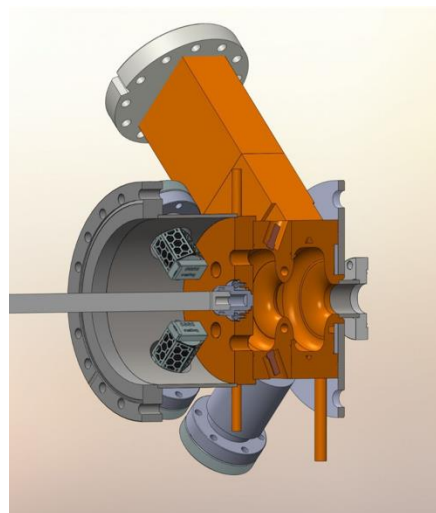
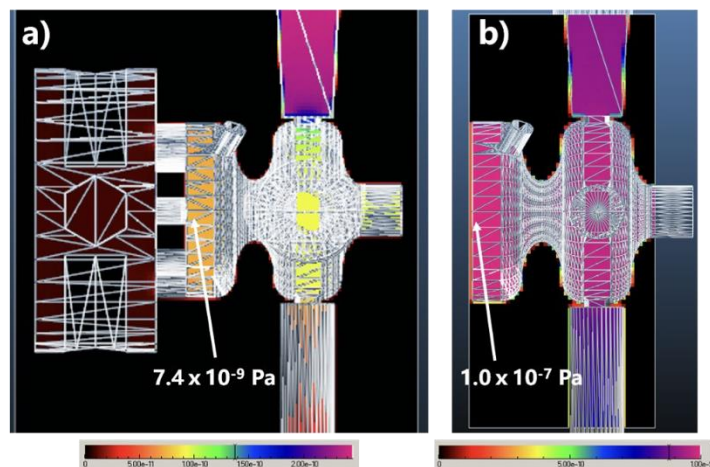


- operating frequency @ 2856 MHz
- High gradient, 100-120MV/m with beam energy >5MeV
- Widely used for high brightness electron beam accelerator, XFEL, ICS, UED, et al.
- copper cathode delivers sub-nC bunch charge
- Cs<sub>2</sub>Te cathode also widely used for long term operation
- Macro pulse repetition rate ~10-100Hz
- Optimized emittance < 0.9  $\mu\text{m}$  @1nC



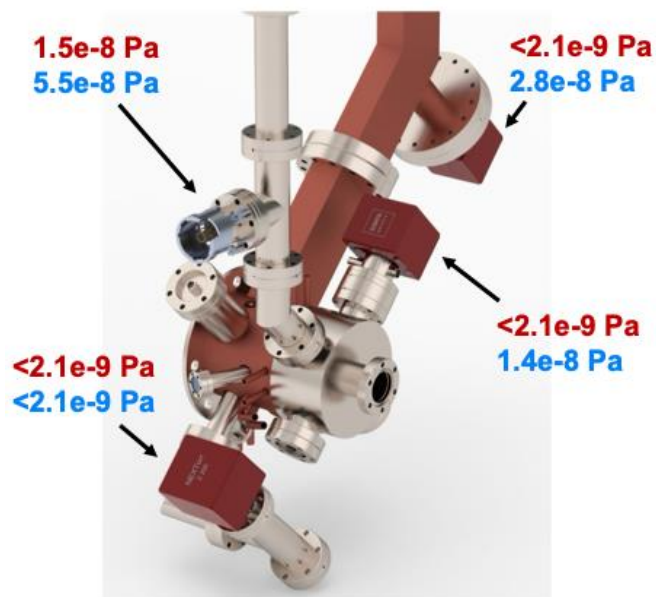


# High vacuum S-band gun at Tsinghua

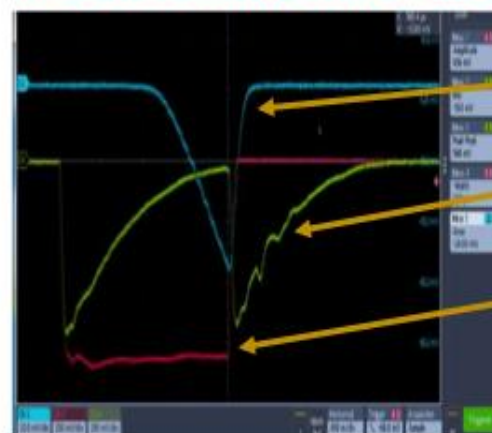


- Special vacuum design based on the normal S-band RF gun
- High gradient,  $\sim 100 \text{ MV/m}$
- good vacuum,  $< 5 \times 10^{-8} \text{ Pa}$  operation pressure
- Operate successfully with semi-conducting photocathode such as Cs<sub>2</sub>Te, K<sub>2</sub>CsSb

## Base/operation pressure



## rf conditioning after 24 hrs

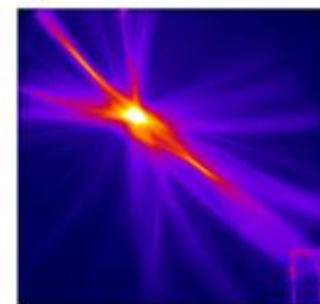


Faraday cup

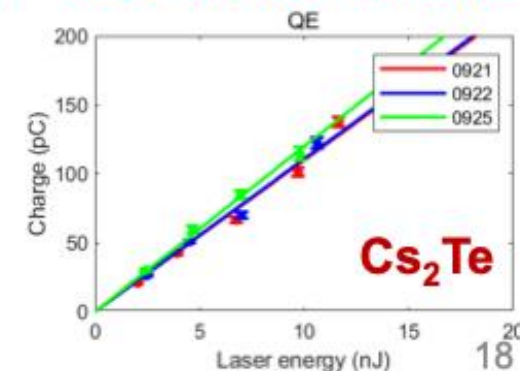
rf in

rf reflec.

Dark current 0.5 nC @  
 $E_z \sim 105 \text{ MV/m}$



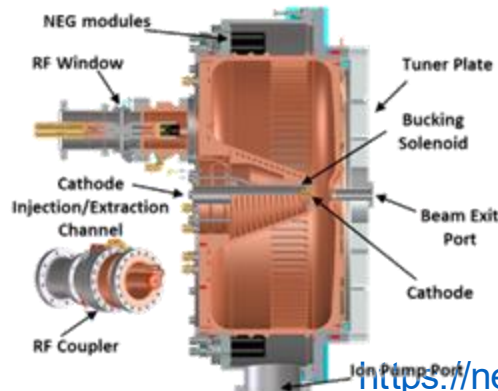
QE  $> \sim 5\%$  over a month





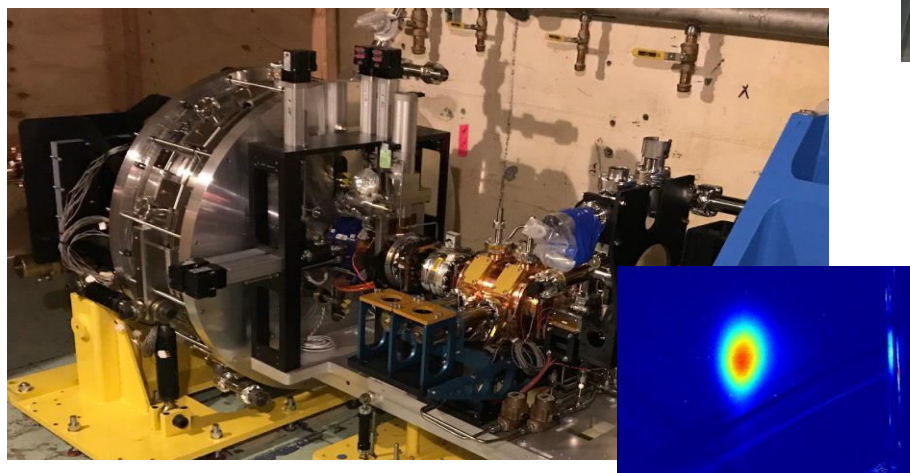


APEX now dedicated for high rep-rate UED



<https://newscenter.lbl.gov/2016/04/26/electron-eye/>

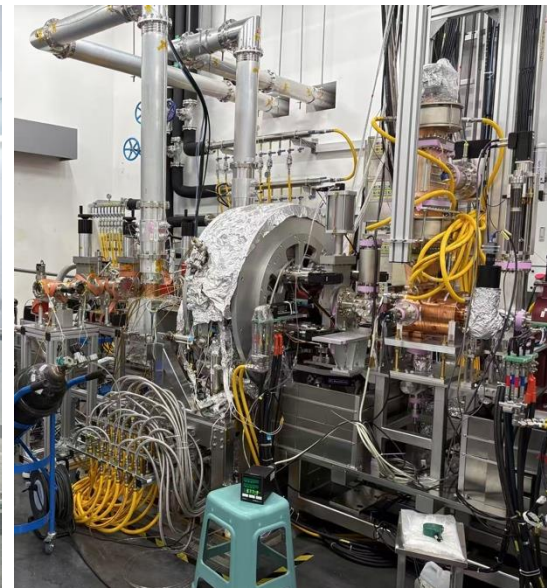
LCLS-II produced first beams in May 2019



SHINE gun



DALS gun

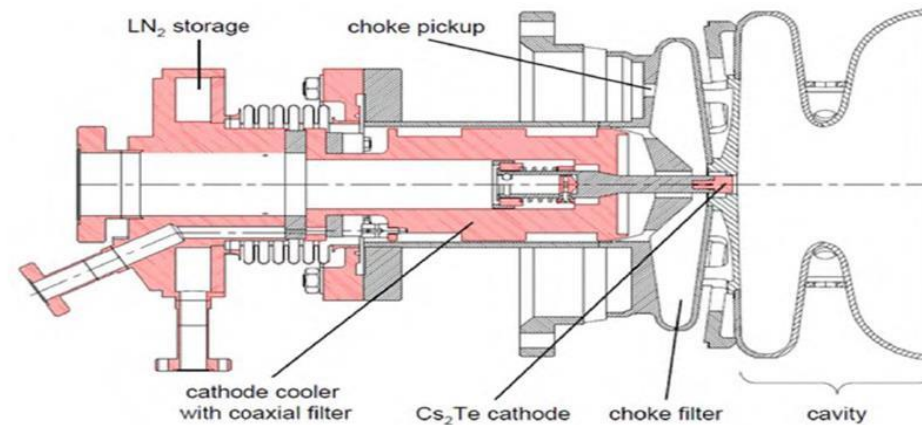
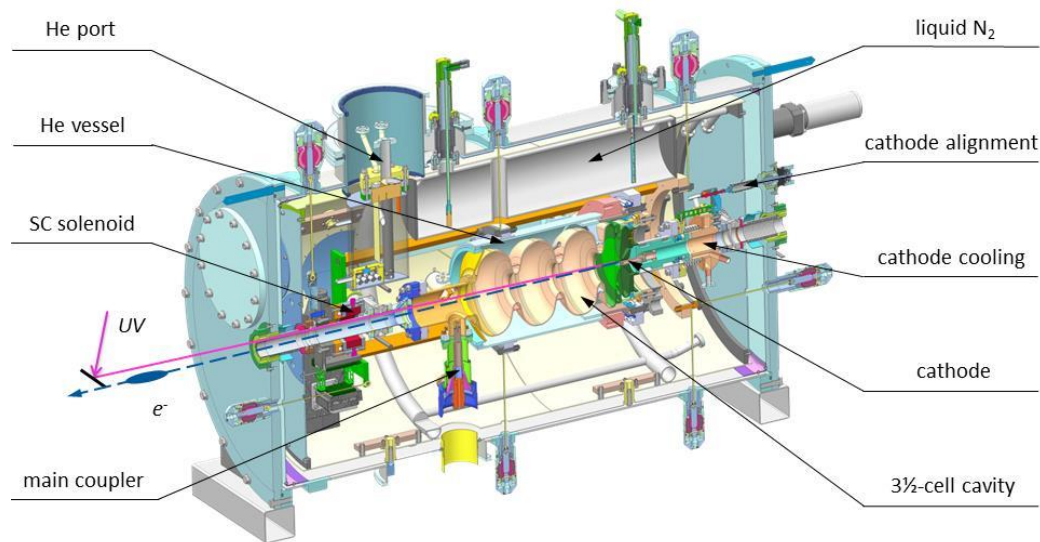


ZjLab gun

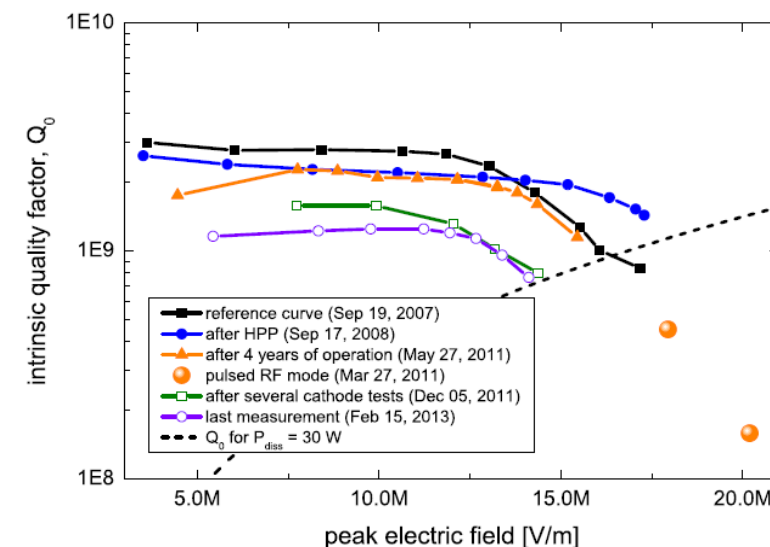


- CW operation with 100uA (100pC/1MHz) in SHINA,DALS, and 3mA successfully are generated in Zjlab.
- Cathode gradient:  $\sim 20\text{-}30\text{MV/m}$ ,  $\sim 750\text{kV}$
- Main Challenge: huge heat load (80-100 kW) and related - material, mechanical, vacuum, lifetime of components etc.



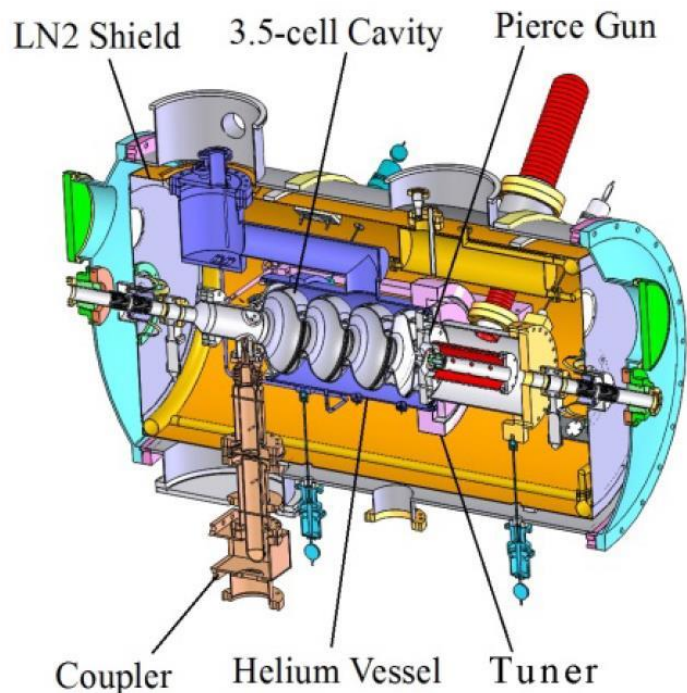


- 1.3 GHz, 3-1/2-cell SRF cavity; 16 MV/m in CW mode; 21.5 MV/m for pulsed rf.
- LN2-cooled Cs<sub>2</sub>Te cathode with rf choke to prevent RF leakage.
- Repetition rate of laser system up to 13 MHz. 20 pC bunch charge.
- Beam energy at 3 MeV in CW mode; 4 MeV in pulsed rf mode.
- 1  $\mu\text{m}/\text{mm}$  beam transverse emittance; energy spread 24 keV.



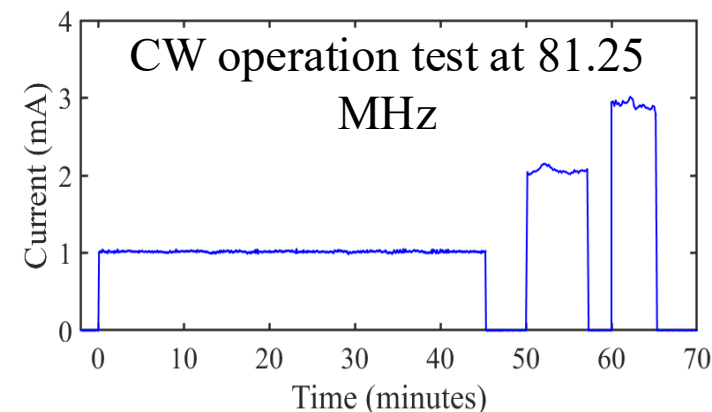
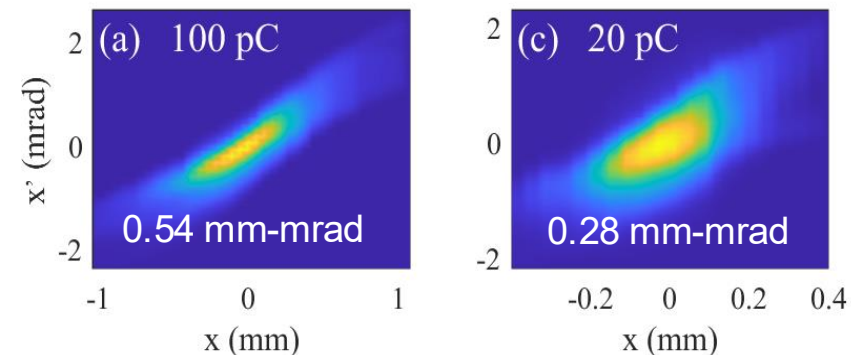


## 2<sup>nd</sup>-generation DC-SRF gun, DC-SRF-II (2017~)



- **Stable CW operation achieved (2023)**  
High-brightness beam test @ 1 MHz  
High average current test @ 81.25 MHz  
Widely tunable current (nA ~ mA)
- **Joint operation with SRF linac at 10 MeV,**  
1 mA, 10% duty factor (2024)
- **DC @ 100 kV; 1.5-cell SRF cavity with**  
 $E_{z,max} \sim 22$  MV/m
- **K<sub>2</sub>CsSb cathode, 515 nm laser + shaping**

DC + SRF



Maximum average beam current ~3 mA; maximum beam power ~5.1 kW



- 1、 Calculate the normalized thermal emittance of a thermionic cathode with cathode temperature  $T$
- 2、 the work function of a photocathode is 4.2eV, is it possible to get photonic emission when a 400nm laser shining on this cathode? If 100MV/m electric field is applied in the gun, the Schottky effect will suppress the barrier, is it possible to get photonic emission with the same laser?